



Table 6-13. Results of the NMU NO_x SIL Modeling Analysis (01-05 SAW MET)

| Averaging Period | NMU Maximum Impact ¹ (µg/m ³) | Year of Maximum Impact | Impact UTM Easting (meters) | Impact UTM Northing (meters) | Significant Impact Level (µg/m ³) | NMU Impact As % Of SIL |
|------------------|--|------------------------|-----------------------------|------------------------------|---|------------------------|
| Annual | 0.974 | 2005 | 468,960.8 | 5,157,154.0 | 1 | 97.40% |

¹ Consistent with how the standards are applied, the maximum annual impact is based upon the highest of the 1st high impacts determined using five discrete years of meteorological data (2001 through 2005).

6.6 TAC MODELING ANALYSIS RESULTS

In addition to the criteria pollutant modeling analyses, a TAC modeling analysis has been conducted to demonstrate that the emissions of TACs from the new CFB boiler (Unit #10) will be in compliance with the Michigan AQD's air toxics regulations. Refined modeling for TACs was performed to determine the ambient, off-property impact from trace metals and organic compounds emitted from the new boiler.

Modeling was performed in accordance with the same methodology used for the criteria pollutant modeling and followed all regulations, guidelines and policies established by U.S. EPA and MDEQ, and again utilized the ISC-AERMOD (PRIME) model Version 04300. Michigan Rule 225 states that emissions from the new or modified source shall not cause a violation of the Initial Threshold Screening Level (ITSL) for non-carcinogens or Initial Risk Screening Level (IRSL) for carcinogenic compounds.

The results were determined by scaling the emission rate for each TAC by model predicted impacts based on a 1.0 gram/second model run for the averaging period associated with each TAC's applicable screening. Using this methodology, it is possible to determine the ambient impacts for multiple pollutants based on one model run instead of running a model for each TAC individually.

The emission rate of each TAC was determined by taking the maximum short term emission rate of each compound for the various fuel types that could potentially be used in the proposed CFB boiler. Table B-2 of Appendix B shows the maximum short term emission rates on a compound-



by-compound basis, which were then converted into gram/second emission rates for scaling purposes. The emission rates and calculated ambient impacts for all TACs (which includes HAPs) are presented in Table C-1 of Appendix C.

The following is a brief description of the procedure for using the gram per second modeled impacts to determine a specific pollutant's maximum ground level concentration.

Worst Case Acetaldehyde Impact, 24-Hour Averaging Period

CFB Boiler Stack Acetaldehyde Emission Rate = 2.47E-02 gram/sec

Gram/Second Modeled Impact for 24-hour averaging period = 1.589 (µg/m³)/(g/sec)

$$\text{Acetaldehyde Impact} = \frac{1.589 (\mu\text{g}/\text{m}^3)}{(1 \text{ gram}/\text{second})} \times \frac{2.47\text{E-}02 \text{ grams}}{\text{second}}$$

$$\text{Acetaldehyde Impact} = \frac{0.0392 \mu\text{g Acetaldehyde}}{\text{m}^3}$$

As shown in the preceding calculations, the acetaldehyde emissions from the new CFB boiler exhaust stack results in a 24-hour impact of 0.0392 µg/m³, which is approximately 0.44% of the acetaldehyde screening level of 9 µg/m³ on a 24-hour basis.

The modeled impacts associated with the annual, 1-hour, 8-hour, and 24-hour modeled averaging periods for the new CFB boiler exhaust stack are presented in Table 6-14.

Table 6-14. 1.0 Gram Per Second Modeled Impacts for the New CFB Boiler

| Averaging Period | Modeled Impact (µg/m ³)/(g/sec) | X (East) Impact Location ¹ (meters) | Y (North) Impact Location ¹ (meters) | Receptor Elevation (meters) |
|------------------|---|--|---|-----------------------------|
| Annual | 0.211 | 468,960.8 | 5,157,204.0 | 193.79 |
| 24-Hour | 1.589 | 468,760.8 | 5,156,254.0 | 201.88 |
| 8-Hour | 2.712 | 466,860.8 | 5,151,904.0 | 283.74 |
| 1-Hour | 15.779 | 466,860.8 | 5,151,904.0 | 283.74 |

¹ These distances are referenced from the site ordinate (UTM coordinate Easting = 468,874.0 meters, and Northing = 5,156,608.0 meters).



Table C-1 of Appendix C presents the results of applying the modeled impacts of Table 6-14 to the maximum TAC emission rates. Table C-1 shows that the TAC emitted at the highest hourly rate, hydrochloric acid (HCl), results in an ambient impact of $0.24 \mu\text{g}/\text{m}^3$ when scaled by the 24-hour modeled impact. This impact is approximately 1.2% of the allowable screening level (SL) of $20 \mu\text{g}/\text{m}^3$ on a 24-hour averaging period basis. Similarly, the TAC that is expected to have the highest ambient impacts versus its screening level is formaldehyde, which has been predicted to result in a maximum annual ambient impact of $0.028 \mu\text{g}/\text{m}^3$ - approximately 34% of the allowable screening level (SL) of $0.08 \mu\text{g}/\text{m}^3$ on an annual averaging period basis. (Note that although the impact for chromium VI is predicted to be approximately 26% of its screening level, the emission rate quantified for Cr VI is uncontrolled and is expected to be much less than the rate presented in Table C-1, and thus result in a much lower impact after considering control efficiency of the baghouse).

Overall, the results presented in Table C-1 show that all TACs will comply with the applicable screening levels at the maximum predicted emission rates and thus comply with the Michigan AQD air toxics rules.

It should be noted that although the Michigan AQD ITSL for lead (Pb) has a 3-month averaging period, a 24-hour ambient impact has been determined and compared to the ITSL of $1.5 \mu\text{g}/\text{m}^3$ on a 3-month basis. This represents a conservative approach because it over predicts the ambient impact that would occur on a 3-month basis.

In conclusion, the proposed operation of the NMU facility expansion will be in compliance with all applicable federal and state ambient air quality standards for both criteria pollutants and TAC emissions.

6.7 DISPERSION MODELING FILES

Table 6-15 lists the ISC AERMOD files that have been included in Appendix C on compact disc. These include the complete Lakes Environmental project files for all modeling runs. The Marquette OE East and Marquette 7.5-minute DEM files utilized in determining elevated terrain through AERMAP are also included electronically.



Table 6-18. Summary of the NMU Modeling Files

| ISC AERMOD View Files | File Description | Meteorological Data |
|---------------------------|--------------------------------------|---------------------|
| NMU01_CO through NMU05_CO | CO SIL Models | 2001-2005 |
| NMUPM_P1 through NMUPM_P5 | PM ₁₀ SIL Models | 2001-2005 |
| NMU01SO2 through NMU05SO2 | SO ₂ PSD and NAAQS Models | 2001-2005 |
| NMU_NOx1 through NMU_NOx5 | NO _x SIL Models | 2001-2005 |
| NMU_GPS2 | TAC modeling Gram/Second Model | 2005 |



7.0 SECONDARY IMPACT ANALYSIS

An additional impact analysis is required for major new sources or major modifications at existing major sources pursuant to 40 CFR Part 52.21(o). In addition, Section 7(a) of the Endangered Species Act (ESA) requires review of threatened and endangered species in the area surrounding the proposed projects. Therefore, the additional impact analysis is necessary to evaluate the impacts from the proposed project on:

- Associated growth
- Soils, vegetation, and wildlife
- Visibility impairment
- Threatened and Endangered Species

The proposed project is considered a major modification and will result in emissions of particulate matter ($PM_{10}/PM_{2.5}$), nitrogen oxides (NO_x), sulfur dioxide (SO_2) and carbon monoxide (CO) greater than the major source significant level. Consequently, an additional impact analysis addressing the effects of PM, NO_x , SO_2 , and CO in these areas is required.

Additionally, MDEQ has requested a quantitative analysis regarding the impact of the 7 MW cooling tower on fogging and icing. Fogging occurs as a result of evaporative moisture from the cooling tower and result in reduced visibility and increased humidity directly adjacent to the cooling tower. Icing when the ambient temperature is below freezing the cooling tower fog freezes on road surfaces.

7.1 ASSOCIATED GROWTH

The purpose of the growth impact analysis is to quantify the impact from growth resulting from the construction and operation of the proposed project and to assess air quality impacts that would result from that growth. Impacts on the ambient air and surrounding community resulting from the installation of the new CFB will be minor.

Northern Michigan University will be receiving solid fuels for the new boiler via 40 ton trucks delivered approximately once per day, Monday through Friday. While an increase in vehicle traffic as a result of fuel truck delivery will increase, both Sugarloaf and Wright Avenues are



currently major transportation routes. Specifically, Sugarloaf Avenue is currently heavily traveled by logging trucks delivering fibers to facilities from processing plants north and west of Marquette. Consequently, the increase in truck traffic as a result of the new solid fuel boiler will be relatively insignificant.

NMU is proposing to construct and install a new CFB boiler and steam turbine in response to increased demand for power and steam at the Marquette campus. The proposed project also includes construction of a new boiler building. Due to abundant supplies of solid fuel, including coal and wood waste, the project is not expected to affect the fuel supply or impact the fuel markets within the upper peninsula of Michigan or the Midwest.

7.2 SOILS, VEGETATION, AND WILDLIFE

Additional increases in pollutant levels resulting from a specific emission source can have an impact on air quality-related values (AQRVs). However, it is important to evaluate the level of the expected increase. AQRVs can include visibility, odor, flora, fauna, and geographic resources; archeological, historical, and other cultural resources; and soil and water resources.

NMU has performed a modeling demonstration for PM₁₀/PM_{2.5}, NO_x, SO₂, and CO emissions resulting from the installation of the new CFB boiler. This ambient impact analysis addressed emissions from the all units at NMU, including the three (3) existing natural gas/oil-fired boilers, and compared the model results with both the primary and secondary National Ambient Air Quality Standards. Note that the primary and secondary standards for PM₁₀, NO_x, SO₂, and CO have the same NAAQS and that the impacts associated with the proposed project will be minor.

The highest predicted NO_x concentration increases resulting from the proposed project at NMU are less than the ambient health standards allowed in the NAAQS. Specifically, AERMOD predicted the following PM₁₀ impacts from the facility as a result of future potential emissions:

- Annual concentration of 0.97 $\mu\text{g}/\text{m}^3$ (primary NAAQS is 100 $\mu\text{g}/\text{m}^3$)



The highest predicted SO₂ concentration increases resulting from the proposed project at NMU are less than the ambient health standards allowed in the NAAQS. Specifically, AERMOD predicted the following PM₁₀ impacts from the facility as a result of future potential emissions:

- 3-hour concentration of 520.24 $\mu\text{g}/\text{m}^3$ (primary NAAQS is 1,300 $\mu\text{g}/\text{m}^3$)
- 24-hour concentration of 217.39 $\mu\text{g}/\text{m}^3$ (primary NAAQS is 365 $\mu\text{g}/\text{m}^3$)
- Annual concentration of 30.56 $\mu\text{g}/\text{m}^3$ (primary NAAQS is 80 $\mu\text{g}/\text{m}^3$)

Modeling was also performed for PM₁₀ and CO emissions. This modeling showed that the impacts from both PM₁₀ and CO as a result of the proposed project are less than the federal significant impact levels of 1 and 5 $\mu\text{g}/\text{m}^3$, and 500 and 2,000 $\mu\text{g}/\text{m}^3$, respectively.

Based on the modeling results presented above, no impact on soils, vegetation, or wildlife can be expected. Further, these small concentration increases are not likely to have an adverse effect on AQRVs within the vicinity of the facility.

7.3 VISIBILITY

NMU is located within 50 km from the Seney National Wildlife Refuge (Seney) Class I area. As such, a visibility analysis using the CALPUFF model was performed to determine whether the emissions from the new CFB will cause a degradation of visibility due to increased relative humidity within Seney.

The visibility modeling demonstration was performed according the modeling protocol submitted to MDEQ on August 18, 2006 and approved via e-mail on August 21, 2006. The results confirm that the potential emissions from the new CFB will not result in visibility impairment at Seney.

While sulfates are a subset of the PM_{2.5} and known to contribute to regional haze problems, the small incremental increase in sulfates from the proposed project are considered to be negligible in comparison to the region's current quality index and have not been quantified. Therefore, no adverse effect on regional haze is expected from the proposed new boiler.



7.4 THREATENED AND ENDANGERED SPECIES

A request for review of threatened and endangered species in the area surrounding the NMU facility was submitted to the Michigan Department of Natural Resources (MDNR) was submitted by NTH Consultants, Ltd. A review by the MDNR – Wildlife Division determined that “the project should have no impact on rare or unique natural features ...” and a copy of the letter from Ms. Lori Sargent, Endangered Species Specialist, is included in Appendix E.

Additionally, a request for review for threatened and endangered species by the U.S. Fish and Wildlife Service was requested as well. Per the letter included in Appendix E, the U.S. Fish and Wildlife Service confirms that no threatened and endangered species are present in the area impacted by the project and no additional review is necessary.

7.5 COOLING TOWER IMPACTS

As requested by MDEQ, a quantitative analysis for impacts of fogging and icing from the proposed 7 MW cooling tower was performed using the Seasonal/Annual Cooling Tower Impact (SACTI) model. This analysis confirmed that impairments to the surrounding community as a result of fogging and icing is not expected. The electronic input and output files from this analysis is included in Appendix C on compact disc, with hardcopy output in Appendix F.



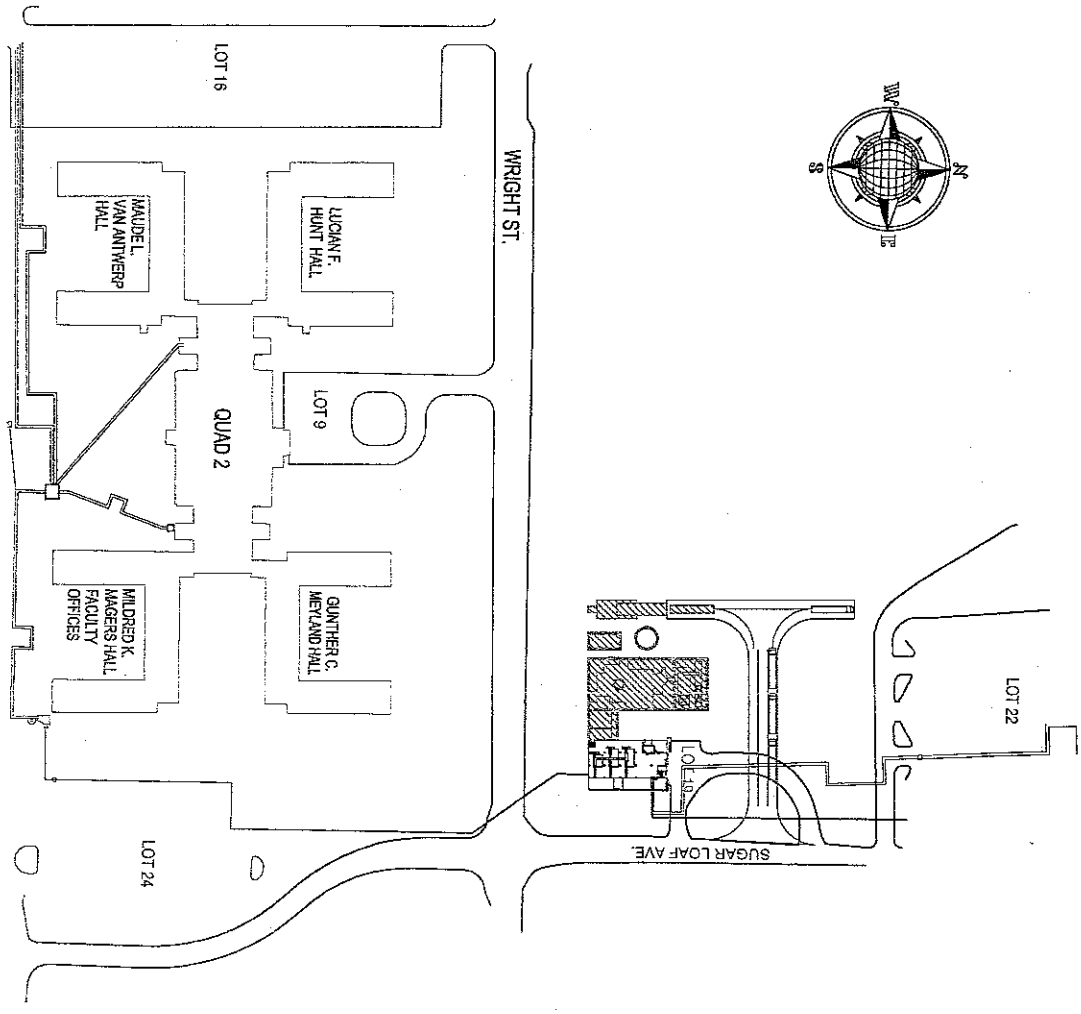
APPENDIX A

Site Drawings

CAMPUS MAP - NORTHERN SECTION

NORTHERN MICHIGAN UNIVERSITY

MARQUETTE, MICHIGAN
 DATE: SEPTEMBER 4, 2003



| ELECTRICAL LEGEND | |
|-------------------|-------------------------|
| SYMBOL | UTILITY |
| — | ELECTRIC |
| ⊛ | HIGH MAST LIGHTPOLE |
| ⊙ | SINGLE SKEWER LIGHTPOLE |
| ⊚ | DOUBLE SKEWER LIGHTPOLE |
| ⊕ | QUAD SKEWER LIGHTPOLE |
| ⊖ | LIGHTPOLE |
| ⊗ | COKE BLUE SWITCH |
| ⊘ | MANHOLE |
| ⊙ | LISTED BUILDING SITES |

| STEAM LEGEND | |
|--------------|-------------------------|
| SYMBOL | UTILITY |
| — | STEAM |
| ○ | ABANDONED STEAM MANHOLE |
| ○ | STEAM VAULT (SV) |



APPENDIX B

Emission Summary Tables

Northern Michigan University
New CFB Boiler
Toxic Air Contaminant Modeling Results

1.0 Gram/Sec Modeled Impacts

| Averaging Period | Impact (ug/m ³ / 1 g/s) |
|------------------|------------------------------------|
| Annual | 0.211 |
| 24 Hour | 1.589 |
| 8 Hour | 2.712 |
| 1 Hour | 15.779 |

Table C-1. TAC Emission Rates and Modeling Impact Results

| Compound | CAS No. | Maximum Emission Rates | | Modeled Rate (gram/sec) | ITSL (ug/m3) | IRSL (ug/m3) | Averaging Period | Ambient Impact (ug/m3) | % of SL |
|--|------------|------------------------|----------|-------------------------|--------------|--------------|------------------|------------------------|---------|
| | | (lb/hr) | (tpy) | | | | | | |
| Lead | 7439-92-1 | 2.48E-03 | 1.09E-02 | 3.12E-04 | 1.5 | | 24 hour | 4.96E-04 | 0.03% |
| HCl | 7647-01-0 | 1.20 | 5.26 | 1.51E-01 | 20 | | 24 hour | 2.41E-01 | 1.20% |
| HF | 7664-39-3 | 0.15 | 0.66 | 1.89E-02 | 26 | | 1 hour | 2.99E-01 | 1.15% |
| H ₂ SO ₄ | 7664-93-9 | 1.13 | 4.94 | 1.42E-01 | 10 | | 8 hour | 3.86E-01 | 3.86% |
| Total Dioxin/Furan | 1746-01-6 | 4.33E-10 | 1.90E-09 | 5.45E-11 | | 2.30E-07 | Annual | 1.15E-11 | 0.00% |
| Metals | | | | | | | | | |
| Antimony | 7440-36-0 | 1.68E-03 | 7.36E-03 | 2.12E-04 | 0.2 | | 24 hour | 3.37E-04 | 0.168% |
| Arsenic | 7440-38-2 | 1.42E-04 | 6.22E-04 | 1.79E-05 | | 0.0002 | Annual | 3.77E-06 | 1.88% |
| Barium | 7440-39-3 | 9.18E-04 | 4.02E-03 | 1.16E-04 | 5 | | 8 hour | 3.14E-04 | 0.006% |
| Beryllium | 7440-41-7 | 3.70E-06 | 1.62E-05 | 4.66E-07 | 0.02 | | 24 hour | 7.41E-07 | 0.004% |
| Beryllium | 7440-41-7 | 3.70E-06 | 1.62E-05 | 4.66E-07 | | 0.0004 | Annual | 9.83E-08 | 0.025% |
| Cadmium | 7440-43-9 | 2.29E-04 | 1.00E-03 | 2.89E-05 | | 0.0006 | Annual | 6.09E-06 | 1.02% |
| Chromium, total | 7440-47-3 | 4.95E-03 | 2.17E-02 | 6.24E-04 | 0.1 | | Annual | 1.31E-04 | 0.131% |
| Chromium, hexavalent | 18540-29-9 | 8.25E-04 | 3.61E-03 | 1.04E-04 | 0.1 | | 24 hour | 1.65E-04 | 0.17% |
| Chromium, hexavalent | 18540-29-9 | 8.25E-04 | 3.61E-03 | 1.04E-04 | | 8.30E-05 | Annual | 2.19E-05 | 26.40% |
| Chromium, trivalent | 18065-83-1 | 1.55E-04 | 6.78E-04 | 1.85E-05 | 5 | | 8 hour | 5.29E-05 | 0.001% |
| Cobalt | 7440-48-4 | 1.25E-03 | 5.48E-03 | 1.58E-04 | 0.2 | | 8 hour | 4.28E-04 | 0.214% |
| Copper | 7440-50-8 | 1.16E-04 | 5.06E-04 | 1.46E-05 | 2 | | 8 hour | 3.95E-05 | 0.002% |
| Iron | | 2.33E-03 | 1.02E-02 | 2.94E-04 | 0.1 | | Annual | 6.20E-05 | 0.06% |
| Magnesium | 7439-95-4 | 1.38E-01 | 6.03E-01 | 1.73E-02 | 100 | | 8 hour | 4.70E-02 | 0.047% |
| Manganese | 7439-96-5 | 3.77E-03 | 1.65E-02 | 4.75E-04 | 0.05 | | 24 hour | 7.55E-04 | 1.51% |
| Molybdenum | | 2.29E-04 | 1.00E-03 | 2.89E-05 | 0.1 | | Annual | 6.09E-06 | 0.006% |
| Nickel | 7440-02-0 | 3.09E-04 | 1.35E-03 | 3.89E-05 | | 0.0042 | Annual | 8.21E-06 | 0.20% |
| Phosphorus | 7723-14-0 | 6.37E-05 | 2.79E-04 | 8.02E-06 | 1 | | 8 hour | 2.17E-05 | 0.002% |
| Potassium | | 9.19E-02 | 4.03E-01 | 1.16E-02 | 0.1 | | Annual | 2.44E-03 | 2.44% |
| Selenium | 7782-49-2 | 1.63E-02 | 7.15E-02 | 2.06E-03 | 2 | | 8 hour | 5.58E-03 | 0.279% |
| Silver | 7440-22-4 | 4.01E-03 | 1.76E-02 | 5.05E-04 | 0.1 | | 8 hour | 1.37E-03 | 1.37% |
| Sodium | | 8.49E-04 | 3.72E-03 | 1.07E-04 | 0.1 | | Annual | 2.25E-05 | 0.02% |
| Strontium | | 2.36E-05 | 1.03E-04 | 2.97E-06 | 0.1 | | Annual | 6.26E-07 | 0.001% |
| Tin | 7440-31-5 | 5.42E-05 | 2.37E-04 | 6.83E-06 | 20 | | 8 hour | 1.85E-05 | 0.000% |
| Titanium | | 4.72E-05 | 2.07E-04 | 5.94E-06 | 0.1 | | Annual | 1.25E-06 | 0.001% |
| Vanadium | | 4.80E-04 | 2.10E-03 | 6.04E-05 | 0.1 | | Annual | 1.27E-05 | 0.013% |
| Yttrium | | 7.07E-07 | 3.10E-06 | 8.91E-08 | 0.1 | | Annual | 1.88E-08 | 0.000% |
| Zinc (as ZnO) | 1314-13-2 | 5.23E-02 | 2.29E-01 | 6.59E-03 | 50 | | 8 hour | 1.79E-02 | 0.036% |
| Organic Toxic Air Contaminants (TACs) | | | | | | | | | |
| Acetaldehyde | 75-07-0 | 1.98E-01 | 8.57E-01 | 2.47E-02 | 9 | | 24 hour | 3.92E-02 | 0.435% |
| Acetaldehyde | 75-07-0 | 1.96E-01 | 8.57E-01 | 2.47E-02 | | 0.5 | Annual | 5.20E-03 | 1.04% |
| Acetophenone | 98-86-2 | 1.88E-04 | 8.22E-04 | 2.37E-05 | 490 | | 8 hour | 6.41E-05 | 0.000% |
| Acrolein | 107-02-8 | 2.39E-02 | 1.05E-01 | 3.01E-03 | 0.02 | | Annual | 6.34E-04 | 3.17% |
| Acrolein | 107-02-8 | 2.39E-02 | 1.05E-01 | 3.01E-03 | 0.5 | | 1 hour | 4.75E-02 | 9.50% |
| Benzene | 71-43-2 | 9.90E-01 | 4.34E+00 | 1.25E-01 | 30 | | 24 hour | 1.98E-01 | 0.66% |
| Benzene | 71-43-2 | 9.90E-01 | 4.34E+00 | 1.25E-01 | | 0.1 | Annual | 2.63E-02 | 26.30% |
| Benzyl chloride | 100-44-7 | 8.76E-03 | 3.84E-02 | 1.10E-03 | | 0.02 | Annual | 2.33E-04 | 1.16% |
| Benzoic acid | 65-85-0 | 1.11E-05 | 4.85E-05 | 1.40E-06 | 0.1 | | Annual | 2.94E-07 | 0.000% |
| Biphenyl | 92-52-4 | 2.13E-05 | 9.32E-05 | 2.68E-06 | 15 | | 8 hour | 7.27E-06 | 0.000% |
| Bis(2-Ethylhexyl)phthalate | 117-81-7 | 9.14E-04 | 4.00E-03 | 1.15E-04 | | 0.2 | Annual | 2.43E-05 | 0.012% |
| Bromoform | 75-25-2 | 4.88E-04 | 2.14E-03 | 6.15E-05 | | 0.9 | Annual | 1.30E-05 | 0.001% |
| Carbon disulfide | 75-15-0 | 1.63E-03 | 7.13E-03 | 2.05E-04 | 700 | | 24 hour | 3.26E-04 | 0.000% |
| Carbazole | 86-74-8 | 4.24E-04 | 1.86E-03 | 5.35E-05 | 0.1 | | Annual | 1.13E-05 | 0.011% |
| Carbon tetrachloride | 56-23-5 | 1.06E-02 | 4.65E-02 | 1.34E-03 | | 0.07 | Annual | 2.82E-04 | 0.40% |
| Chlorine | 7782-50-5 | 1.86E-01 | 8.16E-01 | 2.35E-02 | 15 | | 8 hour | 6.36E-02 | 0.42% |
| 2-Chloroacetophenone | 532-27-4 | 8.76E-05 | 3.84E-04 | 1.10E-05 | 0.03 | | 24 hour | 1.75E-05 | 0.058% |
| Chlorobenzene | 108-90-7 | 7.78E-03 | 3.41E-02 | 9.80E-04 | 70 | | 24 hour | 1.56E-03 | 0.002% |
| Chloroform | 67-66-3 | 6.60E-03 | 2.89E-02 | 8.32E-04 | | 0.4 | Annual | 1.75E-04 | 0.044% |
| 2-Chloronaphthalene | 91-58-7 | 5.66E-07 | 2.48E-06 | 7.13E-08 | 0.1 | | Annual | 1.50E-08 | 0.000% |
| 2-Chlorophenol | 95-57-8 | 5.66E-06 | 2.48E-05 | 7.13E-07 | 0.1 | | Annual | 1.50E-07 | 0.000% |
| Cumene | 98-82-8 | 6.63E-05 | 2.91E-04 | 8.36E-06 | 400 | | 24 hour | 1.33E-05 | 0.000% |
| Cyanide | 57-12-5 | 3.13E-02 | 1.37E-01 | 3.94E-03 | 50 | | 1 hour | 6.22E-02 | 0.12% |
| 1,4-Dichlorobenzene | 106-46-7 | 2.50E-04 | 1.10E-03 | 3.15E-05 | 800 | | 24 hour | 5.01E-05 | 0.000% |
| 1,4-Dichlorobenzene | 106-46-7 | 2.50E-04 | 1.10E-03 | 3.15E-05 | | 0.14 | Annual | 6.65E-06 | 0.005% |
| 2,4-Dinitrophenol | 51-28-5 | 4.24E-05 | 1.86E-04 | 5.35E-06 | 0.1 | | Annual | 1.13E-06 | 0.001% |
| 2,4-Dinitrotoluene | 121-14-2 | 3.50E-06 | 1.53E-05 | 4.42E-07 | 2 | | 8 hour | 1.20E-06 | 0.000% |
| 2,4-Dinitrotoluene | 121-14-2 | 3.50E-06 | 1.53E-05 | 4.42E-07 | | 0.009 | Annual | 9.31E-08 | 0.001% |
| Dimethyl sulfate | 77-78-1 | 6.01E-04 | 2.63E-03 | 7.57E-05 | 0.5 | | 8 hour | 2.05E-04 | 0.041% |
| Ethylbenzene | 100-41-4 | 7.31E-03 | 3.20E-02 | 9.21E-04 | 1000 | | 24 hour | 1.46E-03 | 0.000% |
| Ethylbenzene | 100-41-4 | 7.31E-03 | 3.20E-02 | 9.21E-04 | | 3 | Annual | 1.94E-04 | 0.006% |
| Ethylchloride | 75-00-3 | 5.26E-04 | 2.30E-03 | 6.62E-05 | 10000 | | 24 hour | 1.05E-04 | 0.000% |
| Ethylene dichloride | 107-06-2 | 5.01E-04 | 2.19E-03 | 6.31E-05 | | 0.04 | Annual | 1.33E-05 | 0.033% |
| Ethylene dibromide | 106-93-4 | 1.50E-05 | 6.58E-05 | 1.89E-06 | 9 | | 24 hour | 3.01E-06 | 0.000% |
| Ethylene dibromide | 106-93-4 | 1.50E-05 | 6.58E-05 | 1.89E-06 | | 0.002 | Annual | 3.99E-07 | 0.020% |
| Formaldehyde | 50-00-0 | 1.04E+00 | 4.54E+00 | 1.31E-01 | | 0.08 | Annual | 2.75E-02 | 34.44% |

Northern Michigan University
New CFB Boiler
Toxic Air Contaminant Modeling Results

1.0 Gram/Sec Modeled Impacts

| Averaging Period | Impact (ug/m ³ / 1 g/s) |
|------------------|------------------------------------|
| Annual | 0.211 |
| 24 Hour | 1.589 |
| 8 Hour | 2.712 |
| 1 Hour | 15.779 |

Table C-1. TAC Emission Rates and Modeling Impact Results

| Compound | CAS No. | Maximum Emission Rates | | Modeled Rate (gram/sec) | ITSL (ug/m3) | IRSL (ug/m3) | Averaging Period | Ambient Impact (ug/m3) | % of SL |
|--|------------|------------------------|----------|-------------------------|--------------|--------------|------------------|------------------------|---------|
| | | (lb/hr) | (tpy) | | | | | | |
| Heptachlorobiphenyl | 28655-71-2 | 1.56E-08 | 6.82E-08 | 1.96E-09 | 0.1 | | Annual | 4.13E-10 | 0.000% |
| Hexachlorobiphenyl | 28601-64-9 | 1.30E-07 | 5.68E-07 | 1.63E-08 | 0.1 | | Annual | 3.44E-09 | 0.000% |
| Hexanal | 66-25-1 | 1.65E-03 | 7.23E-03 | 2.08E-04 | 2 | | Annual | 4.38E-05 | 0.002% |
| Hexane | 110-54-3 | 3.75E-01 | 1.64E+00 | 4.73E-02 | 700 | | 24 hour | 7.52E-02 | 0.011% |
| Isobutyraldehyde | 78-84-2 | 2.83E-03 | 1.24E-02 | 3.56E-04 | 160 | | 24 hour | 5.66E-04 | 0.000% |
| Isophorone | 78-59-1 | 7.26E-03 | 3.18E-02 | 9.15E-04 | 280 | | 1 hour | 1.44E-02 | 0.005% |
| Isophorone | 78-59-1 | 7.26E-03 | 3.18E-02 | 9.15E-04 | | 3.7 | Annual | 1.93E-04 | 0.005% |
| 2-Methylnaphthalene | 91-57-6 | 3.77E-05 | 1.65E-04 | 4.75E-06 | 10 | | Annual | 1.00E-06 | 0.000% |
| 3-Methylchloranthrene | | 3.75E-07 | 1.64E-06 | 4.73E-08 | 0.1 | | Annual | 9.97E-09 | 0.000% |
| Monochlorobiphenyl | | 5.19E-08 | 2.27E-07 | 6.25E-09 | 0.1 | | Annual | 1.38E-09 | 0.000% |
| Methyl bromide | 74-83-9 | 3.54E-03 | 1.55E-02 | 4.46E-04 | 5 | | 24 hour | 7.08E-04 | 0.014% |
| Methyl chloride | 74-87-3 | 6.63E-03 | 2.91E-02 | 8.36E-04 | 90 | | 24 hour | 1.33E-03 | 0.001% |
| Methyl chloride | 74-87-3 | 6.63E-03 | 2.91E-02 | 8.36E-04 | | 1.6 | Annual | 1.76E-04 | 0.011% |
| Methyl ethyl ketone | 78-93-3 | 4.88E-03 | 2.14E-02 | 6.15E-04 | 5000 | | 24 hour | 9.77E-04 | 0.000% |
| Methyl hydrazine | 60-34-4 | 2.13E-03 | 9.32E-03 | 2.68E-04 | 0.1 | | Annual | 5.65E-05 | 0.057% |
| Methyl methacrylate | 80-62-6 | 2.50E-04 | 1.10E-03 | 3.15E-05 | 700 | | 24 hour | 5.01E-05 | 0.000% |
| Methyl tert butyl ether | 1634-04-4 | 4.38E-04 | 1.92E-03 | 5.52E-05 | 3000 | | 24 hour | 8.77E-05 | 0.000% |
| Methylene chloride | 75-09-2 | 6.84E-02 | 2.99E-01 | 8.61E-03 | | 2 | Annual | 1.82E-03 | 0.091% |
| Naphthalene | 91-20-3 | 2.29E-02 | 1.00E-01 | 2.88E-03 | 3 | | 24 hour | 4.58E-03 | 0.15% |
| Naphthalene | 91-20-3 | 2.29E-02 | 1.00E-01 | 2.88E-03 | | 0.08 | Annual | 6.07E-04 | 0.76% |
| 2-Nitrophenol | 88-75-5 | 5.66E-05 | 2.48E-04 | 7.13E-06 | 0.1 | | Annual | 1.50E-06 | 0.002% |
| 4-Nitrophenol | 100-02-7 | 2.59E-05 | 1.14E-04 | 3.27E-06 | 0.1 | | Annual | 6.89E-07 | 0.001% |
| Pentachlorobiphenyl | | 2.83E-07 | 1.24E-06 | 3.56E-08 | 0.1 | | Annual | 7.51E-09 | 0.000% |
| Pentachlorophenol | 87-86-5 | 1.20E-05 | 5.27E-05 | 1.51E-06 | 100 | | 24 hour | 2.41E-06 | 0.000% |
| Pentachlorophenol | 87-86-5 | 1.20E-05 | 5.27E-05 | 1.51E-06 | | 0.03 | Annual | 3.19E-07 | 0.001% |
| Perylene | 198-55-0 | 1.23E-07 | 5.37E-07 | 1.54E-08 | 0.1 | | Annual | 3.26E-09 | 0.000% |
| Phenol | 108-95-2 | 1.20E-02 | 5.27E-02 | 1.51E-03 | 600 | | 1 hour | 2.39E-02 | 0.004% |
| Propionaldehyde | 123-38-6 | 1.44E-02 | 6.30E-02 | 1.81E-03 | 4 | | Annual | 3.82E-04 | 0.010% |
| Propanal | 123-38-6 | 7.54E-04 | 3.30E-03 | 9.51E-05 | 4 | | Annual | 2.00E-05 | 0.001% |
| Styrene | 100-42-5 | 4.48E-01 | 1.96E+00 | 5.64E-02 | 1000 | | 24 hour | 8.97E-02 | 0.009% |
| Styrene | 100-42-5 | 4.48E-01 | 1.96E+00 | 5.64E-02 | | 1.7 | Annual | 1.19E-02 | 0.70% |
| Tetrachlorobiphenyl | | 5.89E-07 | 2.58E-06 | 7.43E-08 | 0.1 | | Annual | 1.57E-08 | 0.000% |
| Tetrachloroethylene | 127-18-4 | 8.96E-03 | 3.92E-02 | 1.13E-03 | 0.1 | | Annual | 2.38E-04 | 0.24% |
| Toluene | 108-88-3 | 2.17E-01 | 9.50E-01 | 2.73E-02 | 5000 | | 24 hour | 4.34E-02 | 0.001% |
| o-Tolualdehyde | 529-20-4 | 1.70E-03 | 7.43E-03 | 2.14E-04 | 440 | | 24 hour | 3.40E-04 | 0.000% |
| p-Tolualdehyde | 104-87-0 | 2.59E-03 | 1.14E-02 | 3.27E-04 | 0.1 | | Annual | 6.89E-05 | 0.069% |
| Trichlorobiphenyl | | 6.13E-07 | 2.68E-06 | 7.72E-08 | 0.1 | | Annual | 1.63E-08 | 0.000% |
| Trichlorofluoromethane | 75-69-4 | 9.67E-03 | 4.23E-02 | 1.22E-03 | 56200 | | 1 hour | 1.92E-02 | 0.000% |
| Trichlorethene | 79-01-6 | 7.07E-03 | 3.10E-02 | 8.91E-04 | | 0.6 | Annual | 1.88E-04 | 0.031% |
| 1,1,1-Trichloroethane | 71-55-6 | 7.31E-03 | 3.20E-02 | 9.21E-04 | 1000 | | 24 hour | 1.46E-03 | 0.000% |
| 2,4,6-Trichlorophenol | 88-06-2 | 5.19E-06 | 2.27E-05 | 6.63E-07 | | 0.3 | Annual | 1.38E-07 | 0.000% |
| Vinyl acetate | 108-05-4 | 9.51E-04 | 4.17E-03 | 1.20E-04 | 200 | | 24 hour | 1.90E-04 | 0.000% |
| Vinyl Chloride | 75-01-4 | 4.24E-03 | 1.86E-02 | 5.35E-04 | 100 | | 24 hour | 8.50E-04 | 0.001% |
| Vinyl Chloride | 75-01-4 | 4.24E-03 | 1.86E-02 | 5.35E-04 | | 0.11 | Annual | 1.13E-04 | 0.10% |
| Xylenes | 1330-20-7 | 4.63E-04 | 2.03E-03 | 5.83E-05 | 100 | | 24 hour | 9.27E-05 | 0.000% |
| o-Xylene | 95-47-6 | 5.89E-03 | 2.58E-02 | 7.43E-04 | 100 | | 24 hour | 1.18E-03 | 0.001% |
| Polynuclear Aromatic Hydrocarbons (PAH) | | | | | | | | | |
| Acenaphthene | 83-32-9 | 2.15E-04 | 9.40E-04 | 2.70E-05 | 210 | | 24 hour | 4.30E-05 | 0.000% |
| Acenaphthylene | 208-96-8 | 1.18E-03 | 5.16E-03 | 1.49E-04 | 35 | | 24 hour | 2.36E-04 | 0.001% |
| Acetone | 67-84-1 | 4.48E-02 | 1.96E-01 | 5.64E-03 | 5900 | | 8 hour | 1.53E-02 | 0.000% |
| Anthracene | 120-12-7 | 7.07E-04 | 3.10E-03 | 8.91E-05 | 1000 | | 24 hour | 1.42E-04 | 0.000% |
| Benzaldehyde | 100-52-7 | 2.00E-04 | 8.78E-04 | 2.52E-05 | | 0.4 | Annual | 5.32E-06 | 0.001% |
| Benzo(a)anthracene | 56-55-3 | 1.53E-05 | 6.71E-05 | 1.93E-06 | 0.1 | | Annual | 4.07E-07 | 0.000% |
| Benzo(a)pyrene | 50-32-8 | 6.13E-04 | 2.68E-03 | 7.72E-05 | | 0.0005 | Annual | 1.63E-05 | 3.26% |
| Benzo(b)fluoranthene | 192-97-2 | 6.13E-07 | 2.68E-06 | 7.72E-08 | 0.1 | | Annual | 1.63E-08 | 0.000% |
| Benzo(k)fluoranthene | 205-99-2 | 2.36E-05 | 1.03E-04 | 2.97E-06 | 0.1 | | Annual | 6.26E-07 | 0.001% |
| Benzo(b,j)fluoranthene | 205-82-3 | 8.49E-06 | 3.72E-05 | 1.07E-06 | 0.1 | | Annual | 1.00E-06 | 0.001% |
| Benzo(b,j,k)fluoranthene | | 2.36E-05 | 1.03E-04 | 2.97E-06 | 0.1 | | Annual | 2.25E-07 | 0.000% |
| Benzo(g,h,i)perylene | 191-24-2 | 2.19E-05 | 9.60E-05 | 2.76E-06 | 12 | | Annual | 6.26E-07 | 0.001% |
| Chrysene | 218-01-9 | 8.96E-06 | 3.92E-05 | 1.13E-06 | 0.1 | | 24 hour | 4.39E-06 | 0.000% |
| Crotonaldehyde | 4170-30-3 | 2.33E-03 | 1.02E-02 | 2.94E-04 | 9 | | 1 hour | 4.64E-03 | 0.052% |
| Decachlorobiphenyl | 2051-24-3 | 6.37E-08 | 2.79E-07 | 8.02E-09 | 0.1 | | Annual | 1.69E-09 | 0.000% |
| Dibenzo(a,h)anthracene | 53-70-3 | 2.15E-06 | 9.40E-06 | 2.70E-07 | 0.1 | | Annual | 5.70E-08 | 0.000% |
| 1,2-Dibromoethane | 540-49-8 | 1.30E-02 | 5.68E-02 | 1.63E-03 | 0.1 | | Annual | 3.44E-04 | 0.34% |
| Dichlorobiphenyl | | 1.74E-07 | 7.64E-07 | 2.20E-08 | 0.1 | | Annual | 4.63E-09 | 0.000% |
| 1,2-Dichloroethane | 107-06-2 | 6.84E-03 | 2.99E-02 | 8.61E-04 | | 0.04 | Annual | 1.82E-04 | 0.45% |
| 1,2-Dichloropropane | 78-87-5 | 7.78E-03 | 3.41E-02 | 9.80E-04 | 4 | | 24 hour | 1.56E-03 | 0.039% |
| 7,12-Dimethylbenz(a)anthracene | | 3.34E-06 | 1.46E-05 | 4.20E-07 | 0.1 | | Annual | 8.86E-08 | 0.000% |
| Fluoranthene | 206-44-0 | 3.77E-04 | 1.65E-03 | 4.75E-05 | 140 | | 24 hour | 7.55E-05 | 0.000% |
| Fluorene | 86-73-7 | 8.02E-04 | 3.51E-03 | 1.01E-04 | 140 | | 24 hour | 1.60E-04 | 0.000% |
| Indeno(1,2,3-c,d)pyrene | 193-39-5 | 2.05E-05 | 8.98E-05 | 2.58E-06 | 0.1 | | Annual | 5.45E-07 | 0.001% |
| Phenanthrene | 85-01-8 | 1.65E-03 | 7.23E-03 | 2.08E-04 | 0.1 | | Annual | 4.38E-05 | 0.044% |
| Pyrene | 129-00-0 | 8.72E-04 | 3.82E-03 | 1.10E-04 | 100 | | 24 hour | 1.75E-04 | 0.000% |
| 5-Methyl chrysene | 3697-24-3 | 2.75E-07 | 1.21E-06 | 3.47E-08 | 0.1 | | Annual | 7.31E-09 | 0.000% |

Note: An ITSL of 0.1 that is red bolded is a default screening level per AQD air toxics policy



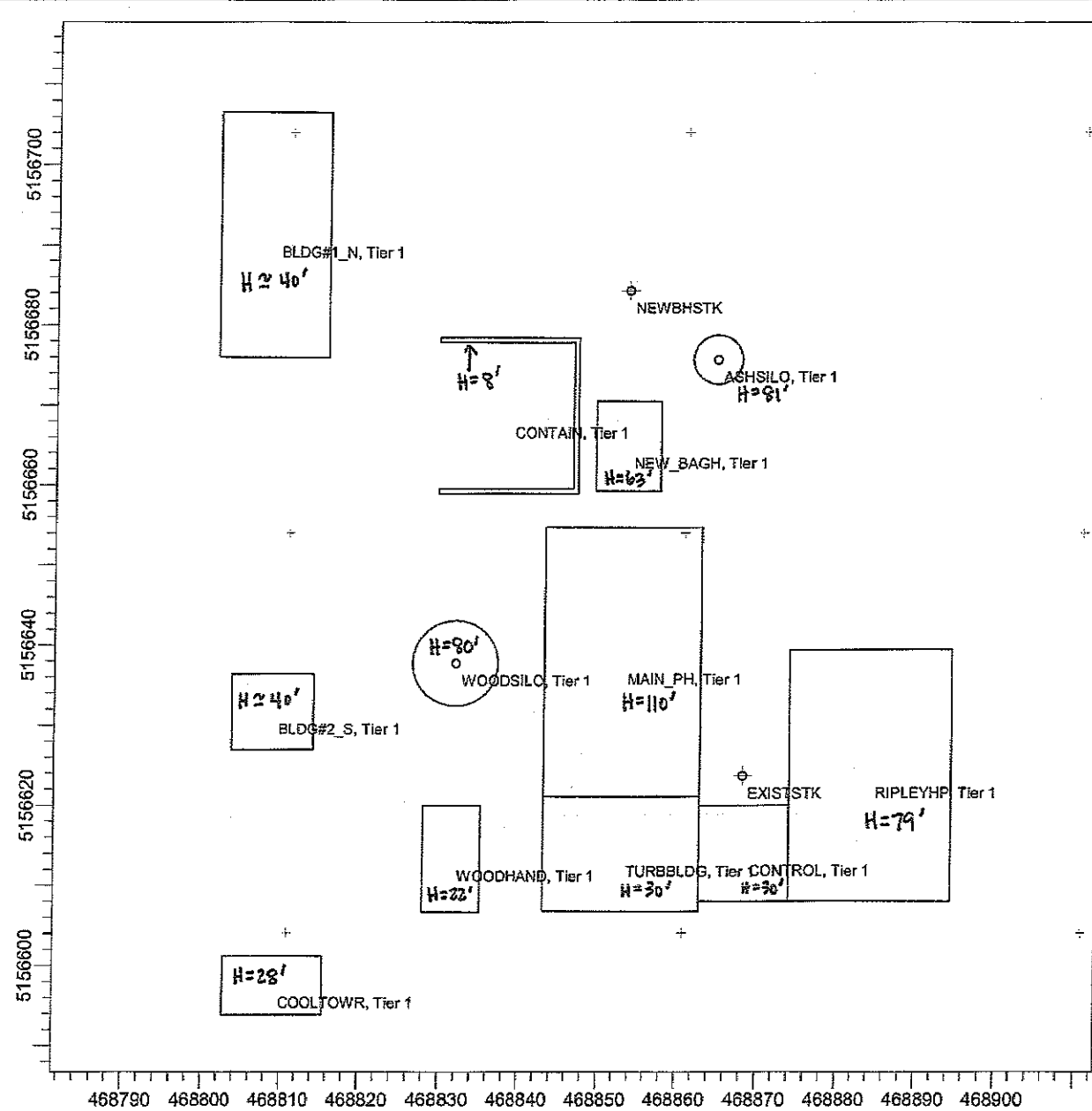
APPENDIX C

Dispersion Modeling Support Information



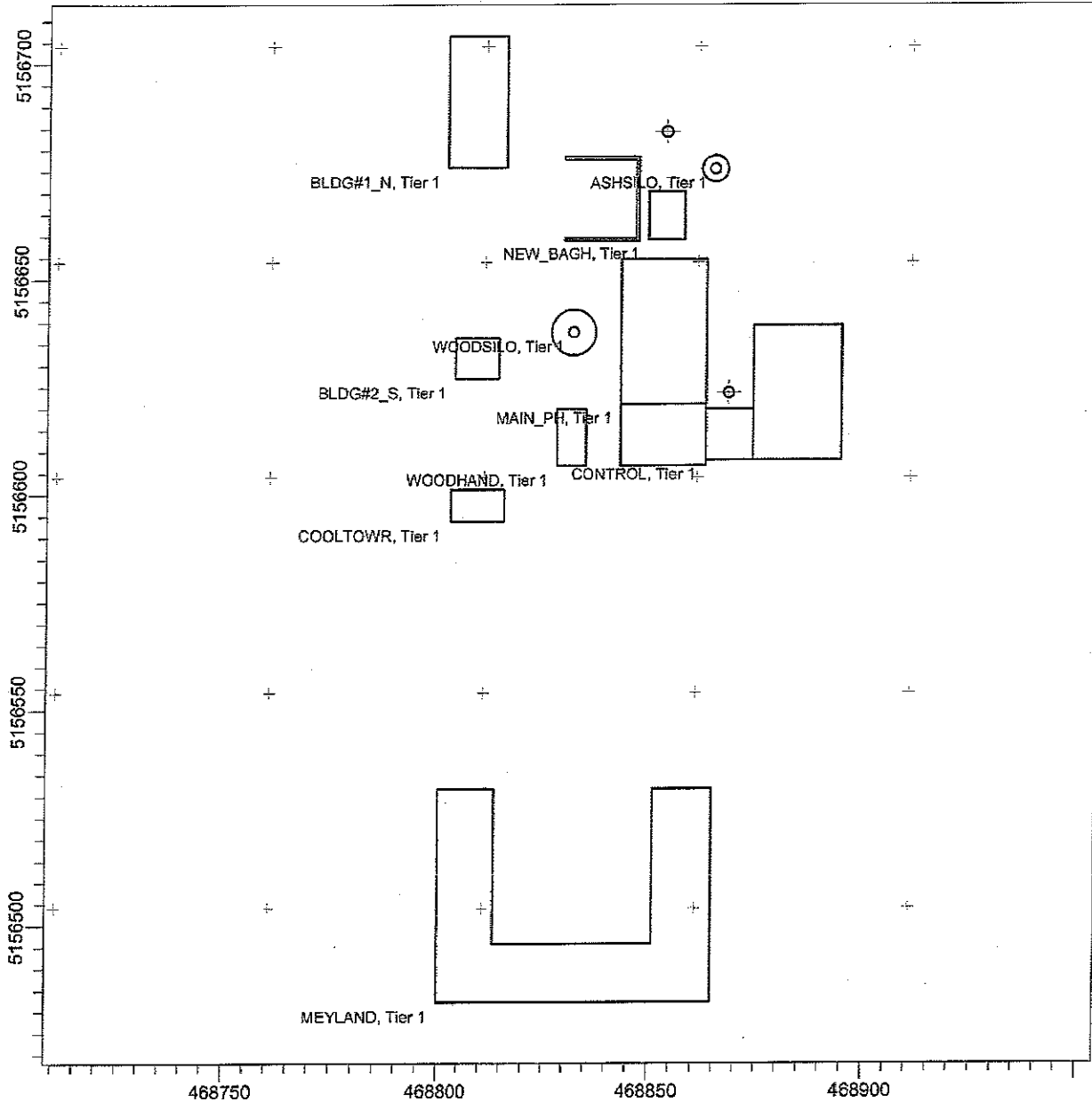
NMU Campus
Modeling Building Layouts
(with Building Heights)


PROJECT TITLE:
Northern Michigan University - Powerhouse Modification PTI
Building Layout



| | | | |
|--|----------------------------------|--|---|
| COMMENTS: NMU Power Plant Building Layout | SOURCES: 2 | COMPANY NAME: NTH Consultants, Ltd | |
| | RECEPTORS: 7537 | MODELER: Edward Bishop, Asst Project Engineer | |
| | | SCALE: 1:800 | |
| | | DATE: 1/25/2007 | PROJECT NO.: 16-060504 |

PROJECT TITLE:
Northern Michigan University - Powerhouse Modification PT1
Building Layout



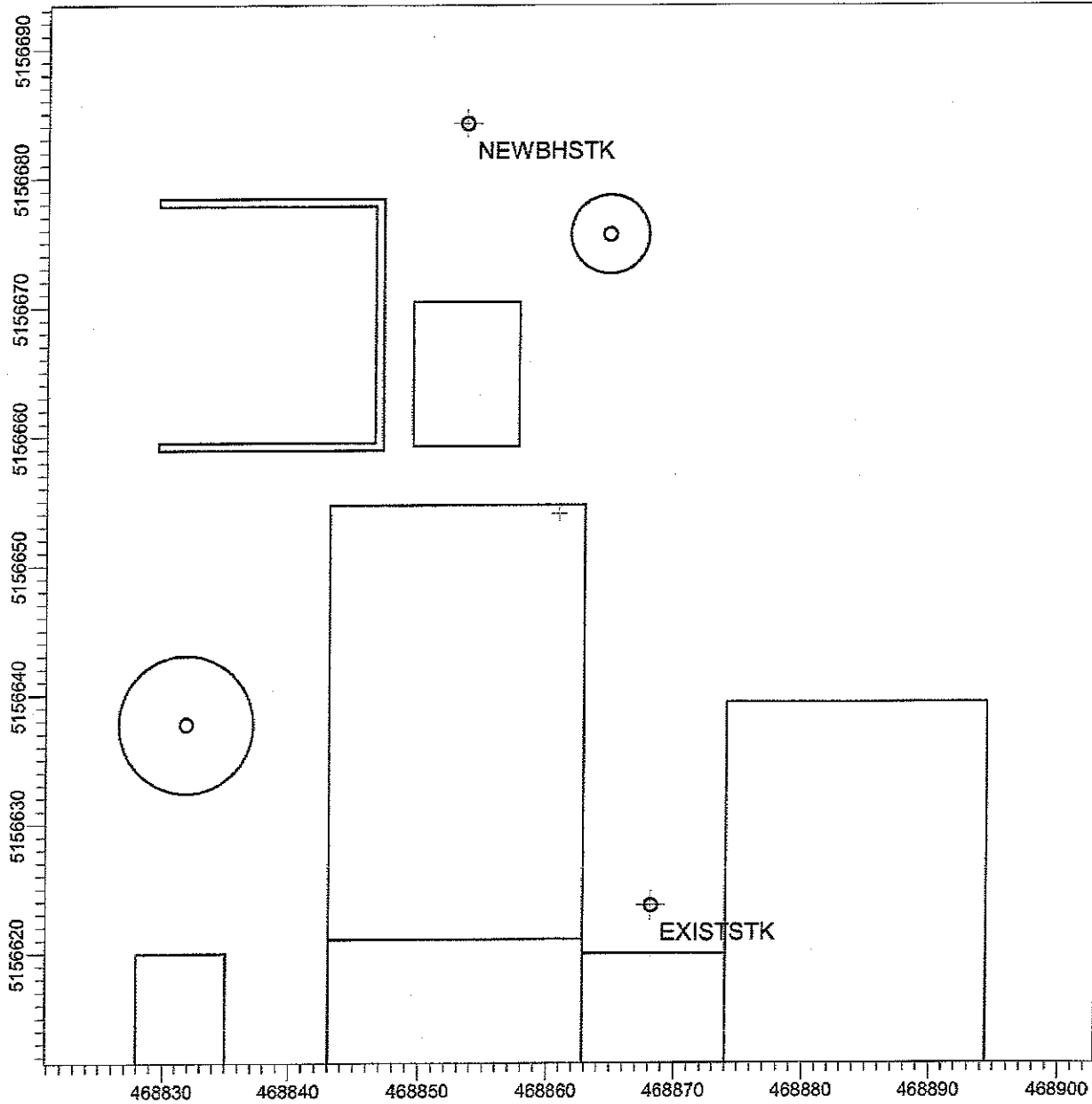
| | | | |
|---|----------------------------------|---|---|
| COMMENTS: NMU Power Plant Building Layout: | SOURCES: 2 | COMPANY NAME: NTH Consultants, Ltd | |
| | RECEPTORS: 7537 | MODELER: Edward Bishop, Asst Project Engineer | |
| | | SCALE: 1:1,500 0  0.05 km | |
| | | DATE: 1/25/2007 | PROJECT NO.: 16-060504 |



Stack Layout

PROJECT TITLE:

**Northern Michigan University - Powerhouse Modification PTI
Stack Identification Layout**



| | | | |
|--|-----------------------------------|---|--|
| <p>COMMENTS: NMU Power Plant Building Layout:</p> | <p>SOURCES: 2</p> | <p>COMPANY NAME: NTH Consultants, Ltd</p> | |
| | <p>RECEPTORS: 7537</p> | <p>MODELER: Edward Bishop, Asst Project Engineer</p> | |
| | | <p>SCALE: 1:500 0 0.01 km</p> | |
| | | <p>DATE: 1/25/2007</p> | <p>PROJECT NO.: 16-060504</p> |



**Existing Facility, New
Structures, and Stack Coordinates
(Internal Coordinates)**

Northern Michigan University - Modeling Analysis Layout for Proposed Boiler Project

Coordinate System Layout for Northern Michigan University Located in Marquette, MI
The Southwest Corner of the Existing Ripley Heating Plant Bldg Equals Site Coordinate (0,0)

| Building | Corner I.D. | Coordinates (feet) | | Height | Coordinates (meters) | | Height | |
|---|-------------|--------------------|---------|--------|----------------------|---------|----------|----------|
| | | X (E) | Y (N) | (feet) | X (E) | Y (N) | (meters) | |
| Ripley Heating Plant | A1 | 0.00 | 0.00 | 79.00 | 0.00 | 0.00 | 24.08 | |
| | A2 | 0.00 | 102.92 | 79.00 | 0.00 | 31.37 | 24.08 | |
| | A3 | 66.92 | 102.92 | 79.00 | 20.40 | 31.37 | 24.08 | |
| | A4 | 66.92 | 0.00 | 79.00 | 20.40 | 0.00 | 24.08 | |
| | A5 | 0.00 | 0.00 | 79.00 | 0.00 | 0.00 | 24.08 | |
| New Boiler Main Building | B1 | -101.53 | 42.82 | 110.00 | -30.95 | 13.05 | 33.53 | |
| | B2 | -101.53 | 153.12 | 110.00 | -30.95 | 46.67 | 33.53 | |
| | B3 | -36.53 | 153.12 | 110.00 | -11.14 | 46.67 | 33.53 | |
| | B4 | -36.53 | 42.82 | 110.00 | -11.14 | 13.05 | 33.53 | |
| | B5 | -101.53 | 42.82 | 110.00 | -30.95 | 13.05 | 33.53 | |
| New Steam Turbine Bldg | C1 | -101.53 | -4.19 | 30.00 | -30.95 | -1.28 | 9.14 | |
| | C2 | -101.53 | 42.82 | 30.00 | -30.95 | 13.05 | 9.14 | |
| | C3 | -36.53 | 42.82 | 30.00 | -11.14 | 13.05 | 9.14 | |
| | C4 | -36.53 | -4.19 | 30.00 | -11.14 | -1.28 | 9.14 | |
| | C5 | -101.53 | -4.19 | 30.00 | -30.95 | -1.28 | 9.14 | |
| New Control Room | D1 | -36.53 | 0.00 | 30.00 | -11.14 | 0.00 | 9.14 | |
| | D2 | -36.53 | 39.13 | 30.00 | -11.14 | 11.93 | 9.14 | |
| | D3 | 0.00 | 39.13 | 30.00 | 0.00 | 11.93 | 9.14 | |
| | D4 | 0.00 | 0.00 | 30.00 | 0.00 | 0.00 | 9.14 | |
| | D5 | -36.53 | 0.00 | 30.00 | -11.14 | 0.00 | 9.14 | |
| Coal Containment Structure | E1 | -145.96 | 167.00 | 8.00 | -44.49 | 50.90 | 2.44 | |
| | E2 | -145.96 | 169.00 | 8.00 | -44.49 | 51.51 | 2.44 | |
| | E3 | -90.29 | 169.00 | 8.00 | -27.52 | 51.51 | 2.44 | |
| | E4 | -90.29 | 229.00 | 8.00 | -27.52 | 69.80 | 2.44 | |
| | E5 | -145.96 | 229.00 | 8.00 | -44.49 | 69.80 | 2.44 | |
| | E6 | -145.96 | 231.00 | 8.00 | -44.49 | 70.41 | 2.44 | |
| | E7 | -88.29 | 231.00 | 8.00 | -26.91 | 70.41 | 2.44 | |
| | E8 | -88.29 | 167.00 | 8.00 | -26.91 | 50.90 | 2.44 | |
| | E9 | -145.96 | 167.00 | 8.00 | -44.49 | 50.90 | 2.44 | |
| Wood Handling Building | F1 | -151.12 | -4.43 | 22.00 | -46.06 | -1.35 | 6.71 | |
| | F2 | -151.12 | 39.14 | 22.00 | -46.06 | 11.93 | 6.71 | |
| | F3 | -127.87 | 39.14 | 22.00 | -38.98 | 11.93 | 6.71 | |
| | F4 | -127.87 | -4.43 | 22.00 | -38.98 | -1.35 | 6.71 | |
| | F5 | -151.12 | -4.43 | 22.00 | -46.06 | -1.35 | 6.71 | |
| New Baghouse Structure | G1 | -80.76 | 168.12 | 63.00 | -24.62 | 51.24 | 19.20 | |
| | G2 | -80.76 | 204.76 | 63.00 | -24.62 | 62.41 | 19.20 | |
| | G3 | -53.75 | 204.76 | 63.00 | -16.38 | 62.41 | 19.20 | |
| | G4 | -53.75 | 168.12 | 63.00 | -16.38 | 51.24 | 19.20 | |
| | G5 | -80.76 | 168.12 | 63.00 | -24.62 | 51.24 | 19.20 | |
| Cooling Tower Structure | H1 | -233.86 | -46.48 | 28.00 | -71.28 | -14.17 | 8.53 | |
| | H2 | -233.86 | -22.48 | 28.00 | -71.28 | -6.85 | 8.53 | |
| | H3 | -191.86 | -22.48 | 28.00 | -58.48 | -6.85 | 8.53 | |
| | H4 | -191.86 | -46.48 | 28.00 | -58.48 | -14.17 | 8.53 | |
| | H5 | -233.86 | -46.48 | 28.00 | -71.28 | -14.17 | 8.53 | |
| Existing Nearby Bldg #1 | I1 | -237.56 | 222.84 | 40.00 | -72.41 | 67.92 | 12.19 | |
| | I2 | -237.56 | 323.23 | 40.00 | -72.41 | 98.52 | 12.19 | |
| | I3 | -191.52 | 323.23 | 40.00 | -58.37 | 98.52 | 12.19 | |
| | I4 | -191.52 | 222.84 | 40.00 | -58.37 | 67.92 | 12.19 | |
| | I5 | -237.56 | 222.84 | 40.00 | -72.41 | 67.92 | 12.19 | |
| Existing Nearby Bldg #2 | J1 | -230.95 | 62.16 | 40.00 | -70.39 | 18.95 | 12.19 | |
| | J2 | -230.95 | 93.06 | 40.00 | -70.39 | 28.37 | 12.19 | |
| | J3 | -196.64 | 93.06 | 40.00 | -59.94 | 28.37 | 12.19 | |
| | J4 | -196.64 | 62.16 | 40.00 | -59.94 | 18.95 | 12.19 | |
| | J5 | -230.95 | 62.16 | 40.00 | -70.39 | 18.95 | 12.19 | |
| Gunther C. Meyland Hall (NE Section of Quad 2) | K1 | -242.84 | -412.65 | 120.00 | -74.02 | -125.78 | 36.58 | |
| | K2 | -242.84 | -250.26 | 120.00 | -74.02 | -76.28 | 36.58 | |
| | K3 | -198.80 | -250.26 | 120.00 | -60.59 | -76.28 | 36.58 | |
| | K4 | -198.80 | -368.41 | 120.00 | -60.59 | -112.29 | 36.58 | |
| | K5 | -75.38 | -368.41 | 120.00 | -22.98 | -112.29 | 36.58 | |
| | K6 | -75.38 | -250.26 | 120.00 | -22.98 | -76.28 | 36.58 | |
| | K7 | -30.78 | -250.26 | 120.00 | -9.38 | -76.28 | 36.58 | |
| | K8 | -30.78 | -412.65 | 120.00 | -9.38 | -125.78 | 36.58 | |
| | K9 | -242.84 | -412.65 | 120.00 | -74.02 | -125.78 | 36.58 | |
| Circular Structures | Center I.D. | Coordinates (feet) | | Height | Coordinates (meters) | | Diameter | Height |
| | | X (E) | Y (N) | (feet) | X (E) | Y (N) | (meters) | (meters) |
| New Ash Silo | O1 | -30.54 | 221.91 | 81.00 | -9.31 | 67.64 | 6.10 | 24.69 |
| Wood Silo | P1 | -138.44 | 97.43 | 80.00 | -42.19 | 29.70 | 10.65 | 24.38 |
| Stacks | I.D. | Coordinates (feet) | | Height | Coordinates (meters) | | Diameter | Height |
| | | X (E) | Y (N) | (feet) | X (E) | Y (N) | (meters) | (meters) |
| New Baghouse Stack | NewBHStk | -67.25 | 250.08 | 165.00 | -20.50 | 76.22 | 1.83 | 50.29 |
| Existing Boiler Stack | ExistStk | -19.02 | 51.28 | 150.00 | -5.80 | 15.63 | 1.52 | 45.72 |



**Existing Facility, New
Structures, and Stack Coordinates
(UTM Coordinates)**

Northern Michigan University - Modeling Analysis Layout for Proposed Boiler Project

**Coordinate System Layout for Northern Michigan University Located in Marquette, MI
The Southwest Corner of the Ripley Heating Plant Bldg Equals UTM Coordinate (468,874 E; 5,156,608 N)**

| Building | Corner I.D. | Coordinates (meters) | | Height (feet) | UTM Coordinates (meters) | | Elevation (meters) |
|---|-------------|----------------------|---------|---------------|--------------------------|------------|--------------------|
| | | X (E) | Y (N) | | Easting | Northing | |
| Ripley Heating Plant | A1 | 0.00 | 0.00 | 79.00 | 468874.00 | 5156608.00 | 195.38 |
| | A2 | 0.00 | 31.37 | 79.00 | 468874.00 | 5156639.37 | 195.38 |
| | A3 | 20.40 | 31.37 | 79.00 | 468894.40 | 5156639.37 | 195.38 |
| | A4 | 20.40 | 0.00 | 79.00 | 468894.40 | 5156608.00 | 195.38 |
| | A5 | 0.00 | 0.00 | 79.00 | 468874.00 | 5156608.00 | 195.38 |
| New Boiler Main Building | B1 | -30.95 | 13.05 | 110.00 | 468843.05 | 5156621.05 | 195.38 |
| | B2 | -30.95 | 46.67 | 110.00 | 468843.05 | 5156654.67 | 195.38 |
| | B3 | -11.14 | 46.67 | 110.00 | 468862.86 | 5156654.67 | 195.38 |
| | B4 | -11.14 | 13.05 | 110.00 | 468862.86 | 5156621.05 | 195.38 |
| | B5 | -30.95 | 13.05 | 110.00 | 468843.05 | 5156621.05 | 195.38 |
| New Steam Turbine Bldg | C1 | -30.95 | -1.28 | 30.00 | 468843.05 | 5156606.72 | 195.38 |
| | C2 | -30.95 | 13.05 | 30.00 | 468843.05 | 5156621.05 | 195.38 |
| | C3 | -11.14 | 13.05 | 30.00 | 468862.86 | 5156621.05 | 195.38 |
| | C4 | -11.14 | -1.28 | 30.00 | 468862.86 | 5156606.72 | 195.38 |
| | C5 | -30.95 | -1.28 | 30.00 | 468843.05 | 5156606.72 | 195.38 |
| New Control Room | D1 | -11.14 | 0.00 | 30.00 | 468862.86 | 5156608.00 | 195.38 |
| | D2 | -11.14 | 11.93 | 30.00 | 468862.86 | 5156619.93 | 195.38 |
| | D3 | 0.00 | 11.93 | 30.00 | 468874.00 | 5156619.93 | 195.38 |
| | D4 | 0.00 | 0.00 | 30.00 | 468874.00 | 5156608.00 | 195.38 |
| | D5 | -11.14 | 0.00 | 30.00 | 468862.86 | 5156608.00 | 195.38 |
| Coal Containment Structure | E1 | -44.49 | 50.90 | 8.00 | 468829.51 | 5156658.90 | 195.38 |
| | E2 | -44.49 | 51.51 | 8.00 | 468829.51 | 5156659.51 | 195.38 |
| | E3 | -27.52 | 51.51 | 8.00 | 468846.48 | 5156659.51 | 195.38 |
| | E4 | -27.52 | 69.80 | 8.00 | 468846.48 | 5156677.80 | 195.38 |
| | E5 | -44.49 | 69.80 | 8.00 | 468829.51 | 5156677.80 | 195.38 |
| | E6 | -44.49 | 70.41 | 8.00 | 468829.51 | 5156678.41 | 195.38 |
| | E7 | -26.91 | 70.41 | 8.00 | 468847.09 | 5156678.41 | 195.38 |
| | E8 | -26.91 | 50.90 | 8.00 | 468847.09 | 5156658.90 | 195.38 |
| | E9 | -44.49 | 50.90 | 8.00 | 468829.51 | 5156658.90 | 195.38 |
| Wood Handling Building | F1 | -46.06 | -1.35 | 22.00 | 468827.94 | 5156606.65 | 195.38 |
| | F2 | -46.06 | 11.93 | 22.00 | 468827.94 | 5156619.93 | 195.38 |
| | F3 | -38.98 | 11.93 | 22.00 | 468835.02 | 5156619.93 | 195.38 |
| | F4 | -38.98 | -1.35 | 22.00 | 468835.02 | 5156606.65 | 195.38 |
| | F5 | -46.06 | -1.35 | 22.00 | 468827.94 | 5156606.65 | 195.38 |
| New Baghouse Structure | G1 | -24.62 | 51.24 | 63.00 | 468849.38 | 5156659.24 | 195.38 |
| | G2 | -24.62 | 62.41 | 63.00 | 468849.38 | 5156670.41 | 195.38 |
| | G3 | -16.38 | 62.41 | 63.00 | 468857.62 | 5156670.41 | 195.38 |
| | G4 | -16.38 | 51.24 | 63.00 | 468857.62 | 5156659.24 | 195.38 |
| | G5 | -24.62 | 51.24 | 63.00 | 468849.38 | 5156659.24 | 195.38 |
| Cooling Tower Structure | H1 | -71.28 | -14.17 | 28.00 | 468802.72 | 5156593.83 | 195.38 |
| | H2 | -71.28 | -6.85 | 28.00 | 468802.72 | 5156601.15 | 195.38 |
| | H3 | -58.48 | -6.85 | 28.00 | 468815.52 | 5156601.15 | 195.38 |
| | H4 | -58.48 | -14.17 | 28.00 | 468815.52 | 5156593.83 | 195.38 |
| | H5 | -71.28 | -14.17 | 28.00 | 468802.72 | 5156593.83 | 195.38 |
| Existing Nearby Bldg #1 | I1 | -72.41 | 67.92 | 40.00 | 468801.59 | 5156675.92 | 196.90 |
| | I2 | -72.41 | 98.52 | 40.00 | 468801.59 | 5156706.52 | 196.90 |
| | I3 | -58.37 | 98.52 | 40.00 | 468815.63 | 5156706.52 | 196.90 |
| | I4 | -58.37 | 67.92 | 40.00 | 468815.63 | 5156675.92 | 196.90 |
| | I5 | -72.41 | 67.92 | 40.00 | 468801.59 | 5156675.92 | 196.90 |
| Existing Nearby Bldg #2 | J1 | -70.39 | 18.95 | 40.00 | 468803.61 | 5156626.95 | 195.38 |
| | J2 | -70.39 | 28.37 | 40.00 | 468803.61 | 5156636.37 | 195.38 |
| | J3 | -59.94 | 28.37 | 40.00 | 468814.06 | 5156636.37 | 195.38 |
| | J4 | -59.94 | 18.95 | 40.00 | 468814.06 | 5156626.95 | 195.38 |
| | J5 | -70.39 | 18.95 | 40.00 | 468803.61 | 5156626.95 | 195.38 |
| Gunther C. Meyland Hall (NE Section of Quad 2) | K1 | -74.02 | -125.78 | 120.00 | 468799.98 | 5156482.22 | 195.38 |
| | K2 | -74.02 | -76.28 | 120.00 | 468799.98 | 5156531.72 | 195.38 |
| | K3 | -60.59 | -76.28 | 120.00 | 468813.41 | 5156531.72 | 195.38 |
| | K4 | -60.59 | -112.29 | 120.00 | 468813.41 | 5156495.71 | 195.38 |
| | K5 | -22.98 | -112.29 | 120.00 | 468851.02 | 5156495.71 | 195.38 |
| | K6 | -22.98 | -76.28 | 120.00 | 468851.02 | 5156531.72 | 195.38 |
| | K7 | -9.38 | -76.28 | 120.00 | 468864.62 | 5156531.72 | 195.38 |
| | K8 | -9.38 | -125.78 | 120.00 | 468864.62 | 5156482.22 | 195.38 |
| | K9 | -74.02 | -125.78 | 120.00 | 468799.98 | 5156482.22 | 195.38 |

Northern Michigan University - Modeling Analysis Layout for Proposed Boiler Project

Coordinate System Layout for Northern Michigan University Located in Marquette, MI
 The Southwest Corner of the Ripley Heating Plant Bldg Equals UTM Coordinate (468,874 E; 5,156,608 N)

| Building | Corner I.D. | Coordinates (meters) | | Height | UTM Coordinates (meters) | | Elevation | |
|-----------------------|--------------|----------------------|-------|--------|--------------------------|--------------|------------|----------|
| | | X (E) | Y (N) | (feet) | Easting | Northing | (meters) | |
| Circular Structures | Center I.D. | Coordinates (feet) | | Height | UTM Coordinates (meters) | | Diameter | Height |
| | | X (E) | Y (N) | (feet) | UTM Easting | UTM Northing | (meters) | (meters) |
| | New Ash Silo | O1 | -9.31 | 67.64 | 81.00 | 468864.69 | 5156675.64 | 6.10 |
| Wood Silo | P1 | -42.19 | 29.70 | 80.00 | 468831.81 | 5156637.70 | 10.65 | 24.38 |
| | | | | | | | | |
| Stacks | I.D. | Coordinates (feet) | | Height | UTM Coordinates (meters) | | Diameter | Height |
| | | X (E) | Y (N) | (feet) | UTM Easting | UTM Northing | (meters) | (meters) |
| New Baghouse Stack | NewBHStk | -20.50 | 76.22 | 165.00 | 468853.50 | 5156684.22 | 1.83 | 50.29 |
| Existing Boiler Stack | ExistStk | -5.80 | 15.63 | 150.00 | 468868.20 | 5156623.63 | 1.52 | 45.72 |

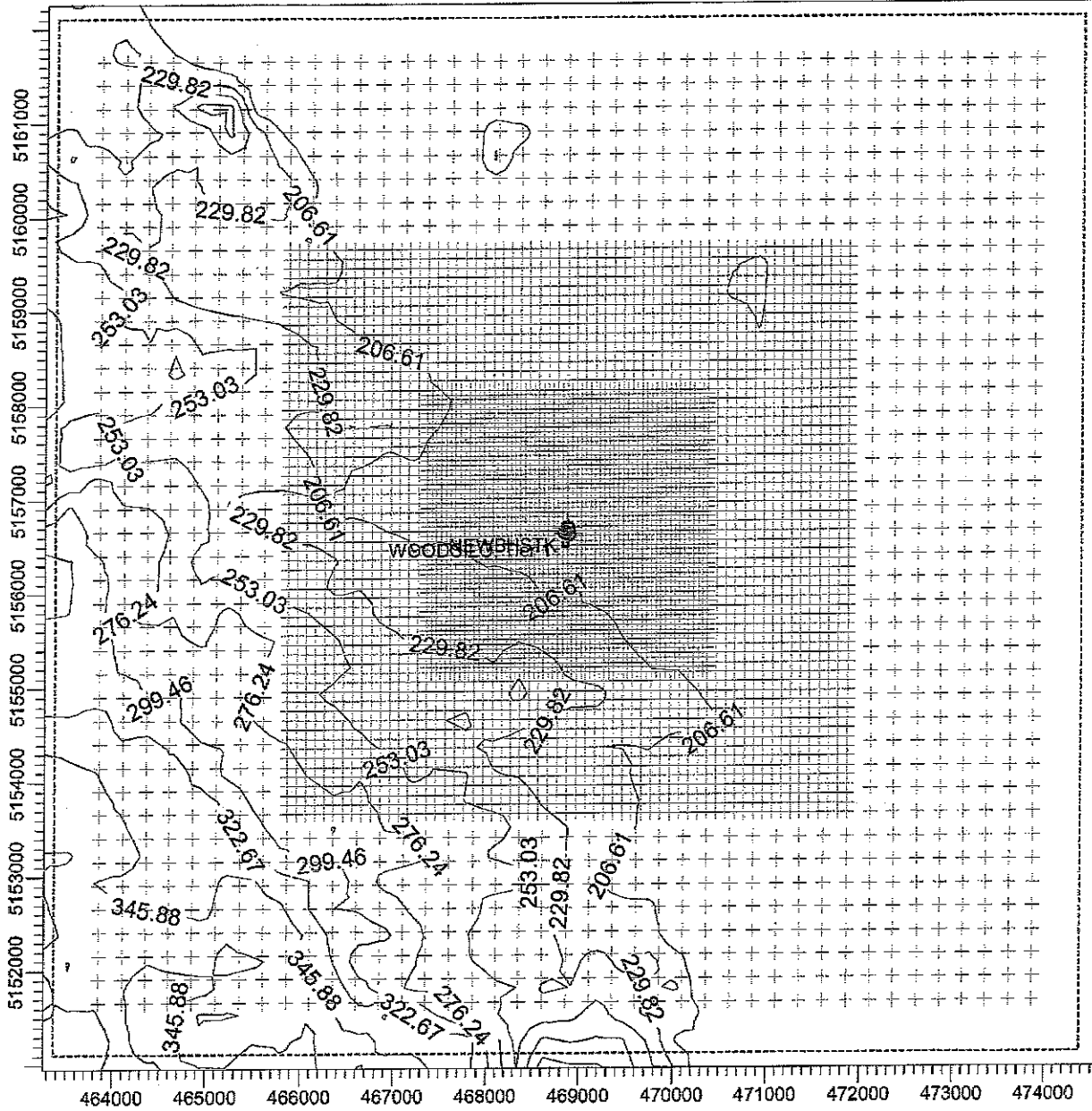
160'
 600"
 Used in modeling inputs



Receptor Grid Layout Diagrams

PROJECT TITLE:

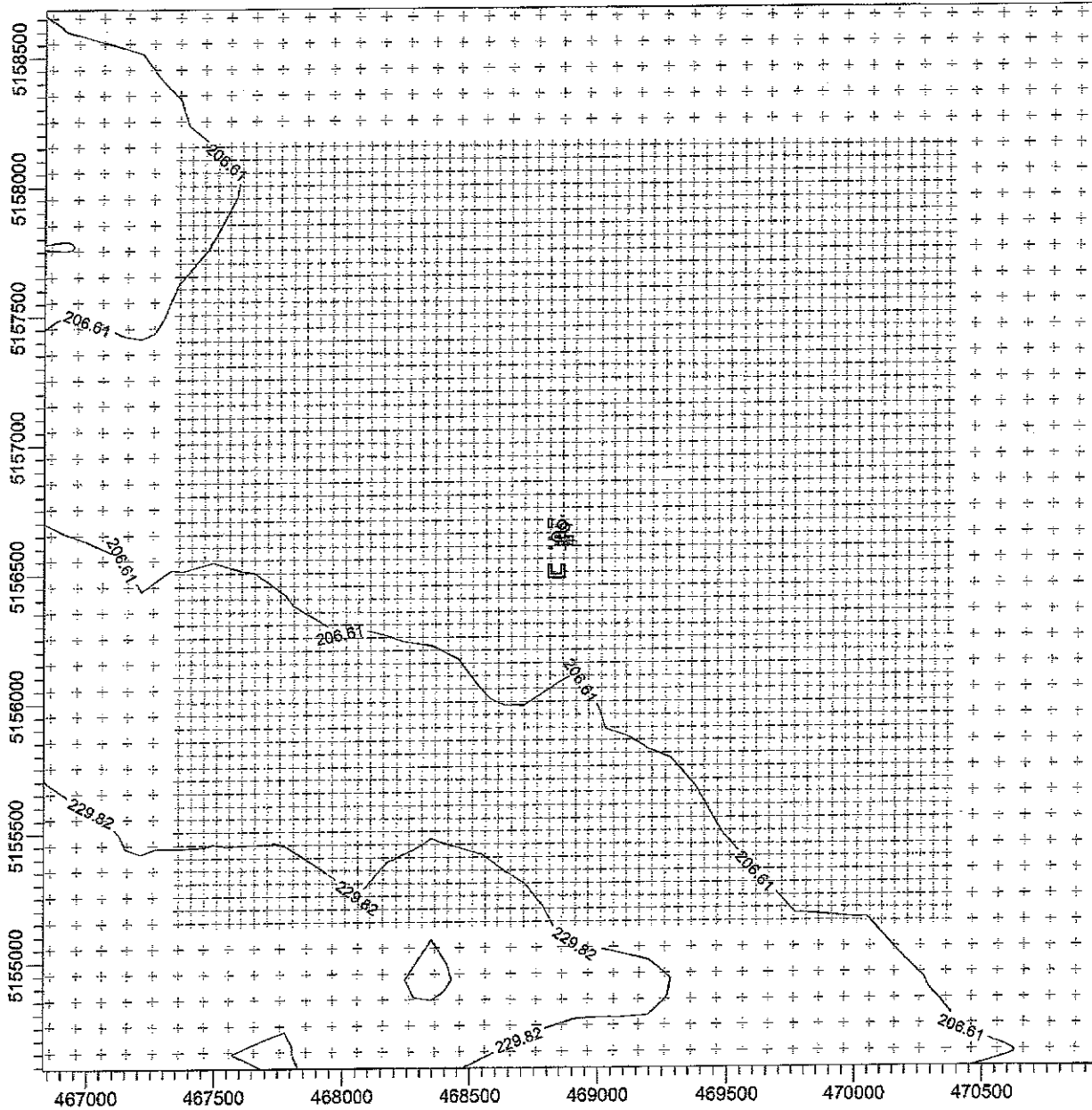
**Northern Michigan University - Powerhouse Modification PTI
Receptor Grid Layout**




| | | | | |
|---|---|---|--|--|
| <p>COMMENTS:</p> <p>NMU Receptor Grid Layout:</p> <p>Inner Grid: 1 km x 1 km 50-m spacing</p> <p>Middle Grid: 3 km x 3 km 100-m spacing</p> <p>Outer Grid: 5 km x 5 km 250-m spacing</p> | <p>SOURCES:</p> <p>2</p> | <p>COMPANY NAME:</p> <p>NTH Consultants, Ltd</p> | | |
| | <p>RECEPTORS:</p> <p>7537</p> | <p>MODELER:</p> <p>Edward Bishop, Asst Project Engineer</p> | | |
| | | <p>SCALE: 1:69,000</p> <p>0 2 km</p> | | |
| | | <p>DATE:</p> <p>1/25/2007</p> | <p>PROJECT NO.:</p> <p>16-060504</p> | |

PROJECT TITLE:

**Northern Michigan University - Powerhouse Modification PTI
Receptor Grid Layout - Zoomed**



| | | | |
|--|---|--|--|
| <p>COMMENTS:</p> <p>NMU Receptor Grid Layout:</p> <p>Inner Grid: 1 km x 1 km 50-m spacing</p> <p>Middle Grid: 3 km x 3 km 100-m spacing</p> | <p>SOURCES:</p> <p>2</p> | <p>COMPANY NAME:</p> <p>NTH Consultants, Ltd</p> | |
| | <p>RECEPTORS:</p> <p>7537</p> | <p>MODELER:</p> <p>Edward Bishop, Asst Project Engineer</p> | |
| | | <p>SCALE: 1:25,000</p> <p>0  0.5 km</p> | |
| | | <p>DATE:</p> <p>1/25/2007</p> | <p>PROJECT NO.:</p> <p>16-060504</p> |



Existing Source Emission Rates

NMU Boiler Project - Existing Source Emission Rates

Pre Permit 126-05 Emission Estimates

Basis: 1,020 Btu/scf nat gas
135,000 Btu/gallon fuel oil

| Year | Nat Gas (MM scf) | Fuel Oil (gal) | Heat Input | | Total (MM Btu) |
|------|---------------------|-------------------|---------------------|----------------------|-------------------|
| | | | Nat Gas (MM Btu) | Fuel Oil (MM Btu) | |
| 2000 | 358.057 | 1313 | 365218 | 177.3 | 365,395 |
| 2001 | 363.993 | 363 | 371212 | 49.0 | 371,261 |
| 2002 | 401.341 | 0 | 409368 | 0.0 | 409,368 |
| 2003 | 377.819 | 22471 | 385375 | 3033.6 | 388,409 |
| 2004 | 384.185 | 25896 | 391869 | 3496.0 | 395,365 |

Potential Fuel Oil Capacity
(MM gally/year)
10,356,267

0.0025 Max Actual Capacity Factor
21.90 Equiv Hrs using Fuel Oil/year

Past Actual - Estimated Annual Emissions

| Pollutant | Tons/Year | | | |
|-----------|-----------|-------|-------|-------|
| | NOx | CO | PM | SO2 |
| 2000 | 17.92 | 15.04 | 1.36 | 0.16 |
| 2001 | 18.20 | 15.29 | 1.38 | 0.12 |
| 2002 | 20.07 | 16.86 | 1.53 | 0.12 |
| 2003 | 19.12 | 15.92 | 1.48 | 0.93 |
| 2004 | 19.47 | 16.20 | 1.51 | 1.06 |
| Maximum | 20.07 | 16.86 | 1.53 | 1.06 |
| lb/hour | 4.582 | 3.848 | 0.348 | 0.242 |

annual average lb/hour

AP42 Factors

| | Nat Gas (lb/mm scf) | Fuel Oil (lb/mmBtu) |
|-----|------------------------|------------------------|
| NOx | 100 | 0.148 |
| CO | 84 | 0.037 |
| PM | 7.6 | 0.03 |
| SO2 | 0.6 | 0.54 |
| VOC | 5.5 | 0.002 |

Permit 126-05 Equipment - Potential Emissions (Based on Two Boilers @ Rated Capacities)

| Pollutant | 2 Boilers Capacity | | Fuel Oil | |
|-----------|--------------------|-------------|-------------|------------|
| | (MM Btu/hr) | (MM scf/hr) | (MM scf/hr) | (gally/hr) |
| Nat Gas | 187.2 | 1,057.14 | | |
| Fuel Oil | 159.6 | | 1,182.22 | 2,732,040 |

Annual Operation With Fuel Type

| | Nat Gas | Fuel Oil |
|-------------|---------|----------|
| (hour/year) | 6449.1 | 2310.9 |

| Pollutant | Potential Emissions (Tons/Year) | | | |
|-----------|---------------------------------|-------|------|-------|
| | NOx | CO | PM | SO2 |
| Nat Gas | 26.43 | 44.40 | 4.02 | 0.32 |
| Fuel Oil | 18.44 | 28.77 | 5.53 | 99.58 |
| Maximum | n/a | n/a | n/a | n/a |
| Totals | 44.87 | 73.17 | 9.55 | 99.90 |

| | Low NOx/AP42 Factors | | Fuel Oil | |
|-----|------------------------|------------------------|------------------------|------------------------|
| | Nat Gas (lb/mm scf) | Fuel Oil (lb/mmBtu) | Nat Gas (lb/mm scf) | Fuel Oil (lb/mmBtu) |
| NOx | 50 | 0.100 | 84 | 0.156 |
| CO | 84 | 0.03 | 7.6 | 0.03 |
| PM | 7.6 | 0.03 | 0.6 | 0.54 |
| SO2 | 0.6 | 0.54 | 5.5 | 0.002 |
| VOC | 5.5 | 0.002 | | |

0.5 Wt-% Sulfur in Fuel Oil

Nat Gas only lb/hour NOx 8.196 CO 13.769 PM 1.246 SO2 0.098 VOC 0.902
 Oil Only (max hourly) lb/hour 15.980 24.898 4.788 86.184 0.319
 Limited Oil Use (annual ave hourly) lb/hr (annual) 10,244 16,705 2,180 22,808 0.748

Note: red bold = maximum emission rate used for future potential modeling purposes

Modeled Emission Rates for Existing Boilers (based on two operating at maximum capacity)

| | NOx | CO | PM | SO2 |
|---------------|-------|-------|--------|--------|
| PSD Increment | 0.714 | 0.559 | 10.829 | |
| NAAQs | 1.291 | 3.137 | 0.603 | 10.859 |

Emission rates above given in units of gram/second



Summary of TAC Analysis Results



Background Concentrations

BACKGROUND (Aug 21 06)

BACKGROUND CONCENTRATIONS

| CITY | ADDRESS | TYPE | YEAR | Distance | 3-HR | 24-HR | ANNUAL |
|--------------|------------------------------------|-------|------|----------|------|-------|--------|
| SO2 Escanaba | County Road 414 | Rural | 2003 | 65.3 km | 45.2 | 13.3 | 2.7 |
| SO2 Escanaba | County Road 414 | Rural | 2004 | 65.3 km | 34.6 | 10.6 | 2.7 |
| SO2 | Seney Nat'l Wildlife Refuge, Hcr2, | Rural | 2005 | 158.5 km | 29.3 | 13.3 | 2.7 |
| | | | | | 45.2 | 13.3 | 2.7 |

| CITY | ADDRESS | TYPE | YEAR | Distance | ANNUAL |
|----------------|-------------------------------------|-------|------|----------|--------|
| NO2 | Harrington Beach State Park, 531 Hw | Rural | 2003 | 225.4 km | 11.5 |
| NO2 Two Rivers | Manitowoc/Woodlnd Dunes, 2315 Goodw | Rural | 2004 | 176.5 km | 5.7 |
| NO2 Two Rivers | Manitowoc/Woodlnd Dunes, 2315 Goodw | Rural | 2005 | 176.5 km | 5.7 |
| | | | | | 11.5 |

| CITY | ADDRESS | TYPE | YEAR | Distance | 24-HR | ANNUAL |
|----------------|---------------------------------|-------|------|----------|----------|--------|
| PM10 Green Bay | Prangeway, 1300 N Quincy Street | Urban | 2003 | 160.8 km | --- | 19.0 |
| PM10 Green Bay | Prangeway, 1300 N Quincy Street | Urban | 2004 | 160.8 km | --- | 15.0 |
| PM10 Green Bay | Prangeway, 1300 N Quincy Street | Urban | 2005 | 160.8 km | --- | 22.0 |
| | | | | | 48.0 | 22.0 |
| | | | | | 4th High | |

| CITY | ADDRESS | TYPE | YEAR | Distance | 1-HR | 8-HR |
|--------------|-------------------------------------|-------|------|----------|------|------|
| CO Milwaukee | Dnr Ser Hdqrts, 2300 N M. I. King J | Urban | 2003 | 258.5 km | 4408 | 3016 |
| CO Milwaukee | Dnr Ser Hdqrts, 2300 N M. I. King J | Urban | 2004 | 258.5 km | 4524 | 3480 |
| CO | Seney Nat'l Wildlife Refuge, Hcr2, | Rural | 2005 | 158.5 km | 812 | 464 |
| | | | | | 4524 | 3480 |

| CITY | ADDRESS | TYPE | YEAR | Distance | QUARTER |
|--------------|---------------------------------|-------|------|----------|---------|
| Pb Milwaukee | Health Center, 1337 So 16th St | Urban | 2003 | 262.1 km | 0.03 |
| Pb | Mayville, Near N6705 Madison Rd | Rural | 2004 | 256.2 km | 0.01 |
| Pb | 1769 S Jeffs Rd | Rural | 2005 | 316.5 km | 0.01 |
| | | | | | 0.03 |



APPENDIX D
RACT/BACT/LAER Clearinghouse Results

Northern Michigan University
RBLC

| RBLCID | FACILITY NAME | STATE | PERMIT No. | PERMIT DATE | DESCRIPTION | PROCESS NAME | FUEL | THRUPUT | UNIT | PROCESS NOTES | POLLUTANT | EMIS LIMIT | UNIT | AVG TIME | BASIS |
|---------|---|-------|--------------|-------------|--|--------------------|---------|---------|---------|---|----------------------------------|------------|----------|------------------------|----------|
| MN-0058 | VIRGINIA DEPARTMENT OF PUBLIC UTILITIES | MN | 13700028-005 | 6/30/2005 | | BOILER, WOOD FIRED | WOOD | 230 | mmbtu/h | | Particulate Matter (PM) | 0.025 | LB/MMBTU | 3-HR TEST | BACT-PSD |
| MN-0068 | VIRGINIA DEPARTMENT OF PUBLIC UTILITIES | MN | 13700028-005 | 6/30/2005 | | BOILER, WOOD FIRED | WOOD | 230 | mmbtu/h | | Particulate Matter < 10 µ (PM10) | 0.025 | LB/MMBTU | 3-HR TEST | BACT-PSD |
| MN-0053 | VIRGINIA DEPARTMENT OF PUBLIC UTILITIES | MN | 13700028-005 | 6/30/2005 | | BOILER, WOOD FIRED | WOOD | 230 | mmbtu/h | | Carbon Monoxide | 0.3 | LB/MMBTU | 4-HOUR BLOCK AVERAGE | BACT-PSD |
| MN-0053 | VIRGINIA DEPARTMENT OF PUBLIC UTILITIES | MN | 13700028-005 | 6/30/2005 | WOOD FIRED BOILER, 230 MMSTU/H HEAT INPUT, SPREADER STOKER | BOILER, WOOD FIRED | WOOD | 230 | mmbtu/h | | Nitrogen Oxides (NOx) | 0.15 | LB/MMBTU | 30 DAY AVERAGE | BACT-PSD |
| MN-0059 | HIBBING PUBLIC UTILITIES | MN | 13700027-003 | 6/30/2005 | | BOILER, WOOD FIRED | WOOD | 230 | mmbtu/h | | Particulate Matter < 10 µ (PM10) | 0.025 | LB/MMBTU | 3-HR TEST | BACT-PSD |
| MN-0059 | HIBBING PUBLIC UTILITIES | MN | 13700027-003 | 6/30/2005 | | BOILER, WOOD FIRED | WOOD | 230 | mmbtu/h | | Particulate Matter (PM) | 0.025 | LB/MMBTU | 3-H TEST | BACT-PSD |
| MN-0059 | HIBBING PUBLIC UTILITIES | MN | 13700027-003 | 6/30/2005 | | BOILER, WOOD FIRED | WOOD | 230 | mmbtu/h | | Carbon Monoxide | 0.3 | LB/MMBTU | 4-HOUR BLOCK AVERAGE | BACT-PSD |
| MN-0059 | HIBBING PUBLIC UTILITIES | MN | 13700027-003 | 6/30/2005 | | BOILER, WOOD FIRED | WOOD | 230 | mmbtu/h | | Nitrogen Oxides (NOx) | 0.15 | LB/MMBTU | 30-DAY ROLLING AVERAGE | BACT-PSD |
| ND-0020 | RICHARDTON PLANT | ND | 4004 | 8/4/2004 | | BOILER, COAL-FIRED | LIGNITE | 250 | MMSTU/H | | Particulate Matter < 10 µ (PM10) | 0.02 | LB/MMBTU | 3-HOUR AVERAGE | BACT-PSD |
| ND-0020 | RICHARDTON PLANT | ND | 4004 | 8/4/2004 | | BOILER, COAL-FIRED | LIGNITE | 250 | MMSTU/H | | Sulfur Oxides (SOx) | 0.03 | LB/MMBTU | 30 DAY ROLLING AVG. | BACT-PSD |
| ND-0020 | RICHARDTON PLANT | ND | 4004 | 8/4/2004 | | BOILER, COAL-FIRED | LIGNITE | 250 | MMSTU/H | | Nitrogen Oxides (NOx) | 0.1 | LB/MMBTU | 30 DAY ROLLING AVERAGE | BACT-PSD |
| ND-0020 | RICHARDTON PLANT | ND | 4004 | 8/4/2004 | | BOILER, COAL-FIRED | LIGNITE | 250 | MMSTU/H | | Carbon Monoxide | 0.11 | LB/MMBTU | 3 HOUR ROLLING AVERAGE | BACT-PSD |
| ND-0020 | RICHARDTON PLANT | ND | 4004 | 8/4/2004 | ETHANOL PRODUCTION PLANT RATED AT 65 MILLION GALLONS PER YEAR. | BOILER, COAL-FIRED | LIGNITE | 250 | MMSTU/H | BOILER ACTS AS A CONTROL DEVICE FOR THE DISTILLERS GRAIN DRYERS, DISTILLATION COLUMNS AND BIONETHANATOR (IE. GASES FROM THESE PROCESSES ARE ROUTED TO THE BOILER FOR COMBUSTION). | Particulate Matter (PM) | 0.048 | LB/MMBTU | 3 HOUR AVERAGE | BACT-PSD |
| ND-0020 | RICHARDTON PLANT | ND | 4004 | 8/4/2004 | | DDGS COOLING | | 22 | T/H | | Particulate Matter < 10 µ (PM10) | 0.004 | GR/DSCF | 3 HOUR AVERAGE | BACT-PSD |
| ND-0020 | RICHARDTON PLANT | ND | 4004 | 8/4/2004 | | GRAIN RECEIVING | | 420 | T/H | | Particulate Matter < 10 µ (PM10) | 0.004 | GR/DSCF | 3 HOUR AVERAGE | BACT-PSD |
| ND-0020 | RICHARDTON PLANT | ND | 4004 | 8/4/2004 | | HAMMERMILLING | | 76 | T/H | | Particulate Matter < 10 µ (PM10) | 0.004 | GR/DSCF | 3 HOUR AVERAGE | BACT-PSD |
| ND-0020 | RICHARDTON PLANT | ND | 4004 | 8/4/2004 | | DDGS LOADOUT | | 420 | T/H | | Particulate Matter < 10 µ (PM10) | 0.004 | GR/DSCF | 3 HOUR AVERAGE | BACT-PSD |
| ND-0020 | RICHARDTON PLANT | ND | 4004 | 8/4/2004 | | COAL HANDLING | | 27 | T/H | | Particulate Matter < 10 µ (PM10) | 0.004 | GR/DSCF | 3 HOUR AVERAGE | BACT-PSD |

| RBLCID | FACILITY NAME | STATE | PERMIT NO. | PERMIT DATE | DESCRIPTION | PROCESS NAME | FUEL | THRUPUT | UNIT | PROCESS NOTES | POLLUTANT | EMIS LIMIT | UNIT | AVG TIME | BASIS |
|---------|----------------------------------|-------|------------|-------------|--|----------------------------|----------------|---------|---------|--|----------------------------------|------------|----------|-------------|----------|
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | <p>THIS FACILITY BREWS AND PACKAGES BEER. EACH BOILER NOT TO EXCEED 180,000 LB STEAM/H OR 238 MMBTU/H BOTH BOILERS TOGETHER NOT TO EXCEED 125,682 TONS COAL/ROLLING 12-MONTHS. THIS PT., 14-05515 IS A MODIFICATION TO PTI #14-05143 ISSUED 11/15/01 FOR THE ADDITION OF AN 8.5 MW STEAM TURBINE GENERATOR TO AN EXISTING COAL FIRED BOILER (THERE WERE NO EMISSIONS FROM THE STEAM TURBINE ITSELF). THIS MODIFICATION WAS TO INCREASE THE HCL HOURLY AND 7YR LIMITS AND SO2/MMBTU LIMIT. THE 7YR FACILITYWIDE LIMITS HAVE NOT CHANGED, EXCEPT FOR HCL WHICH HAS INCREASED BY 46.1 TYS IN THIS NEW PERMIT.</p> | BOILER (2), COAL FIRED | COAL | 238 | MMBTU/H | TWO BOILERS, CAPABLE OF BURNING AND WITH NATURAL GAS. NUMBERS 2 AND 6 FUEL OILS, FOUND PER HOUR LIMITS ARE FOR EACH BOILER, AND EXCEPT FOR VOC AND CO, ALL 7YR LIMITS ARE FOR BOTH BOILERS COMBINED. COAL USAGE FOR BOTH BOILERS TOGETHER NOT TO EXCEED 125,682 TONS/ROLLING 12 MONTHS. THESE LIMITS FOR THE COAL. | Nitrogen Oxides (NOx) | 0.7 | LB/MMBTU | | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), COAL FIRED | COAL | 238 | MMBTU/H | | Carbon Monoxide | 5.2 | LB/H | EACH BOILER | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), COAL FIRED | COAL | 238 | MMBTU/H | | Sulfur Dioxide (SO2) | 1.6 | LB/MMBTU | | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), COAL FIRED | COAL | 238 | MMBTU/H | | Particulate Matter < 10 µ (PM10) | 0.01 | GR/ACF | | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NO. 6 FUEL OIL | NO. 6 FUEL OIL | 238 | MMBTU/H | | Particulate Matter < 10 µ (PM10) | 0.01 | GR/ACF | | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NO. 6 FUEL OIL | NO. 6 FUEL OIL | 238 | MMBTU/H | | Nitrogen Oxides (NOx) | 0.7 | LB/MMBTU | | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NO. 6 FUEL OIL | NO. 6 FUEL OIL | 238 | MMBTU/H | | Carbon Monoxide | 8.15 | LB/H | EACH BOILER | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NO. 6 FUEL OIL | NO. 6 FUEL OIL | 238 | MMBTU/H | | Sulfur Dioxide (SO2) | 1.6 | LB/MMBTU | | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NO. 2 FUEL OIL | NO. 2 FUEL OIL | 238 | MMBTU/H | | Particulate Matter < 10 µ (PM10) | 0.01 | GR/ACF | | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NO. 2 FUEL OIL | NO. 2 FUEL OIL | 238 | MMBTU/H | | Nitrogen Oxides (NOx) | 0.7 | LB/MMBTU | | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NO. 2 FUEL OIL | NO. 2 FUEL OIL | 238 | MMBTU/H | | Volatile Organic Compounds (VOC) | 0.38 | LB/H | EACH BOILER | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NO. 2 FUEL OIL | NO. 2 FUEL OIL | 238 | MMBTU/H | | Carbon Monoxide | 8.5 | LB/H | EACH BOILER | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NATURAL GAS | NATURAL GAS | 238 | MMBTU/H | | Sulfur Dioxide (SO2) | 1.6 | LB/MMBTU | | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NATURAL GAS | NATURAL GAS | 238 | MMBTU/H | | Particulate Matter < 10 µ (PM10) | 0.01 | GR/ACF | | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NATURAL GAS | NATURAL GAS | 238 | MMBTU/H | | Nitrogen Oxides (NOx) | 0.7 | LB/MMBTU | | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | | BOILER (2), NATURAL GAS | NATURAL GAS | 238 | MMBTU/H | | Carbon Monoxide | 20 | LB/H | EACH BOILER | BACT-PSD |
| OH-0241 | MILLER BREWING COMPANY - TRENTON | OH | 14-05515 | 5/27/2004 | BOILER (2), NATURAL GAS | NATURAL GAS | 238 | MMBTU/H | | Sulfur Dioxide (SO2) | 1.6 | LB/MMBTU | | BACT-PSD | |

Northern Michigan University
RBLC

| RBLCID | FACILITY NAME | STATE | PERMIT No. | PERMIT DATE | DESCRIPTION | PROCESS NAME | FUEL | THRUPUT | UNIT | PROCESS NOTES | POLLUTANT | EMIS LIMIT | UNIT | AVG TIME | BASIS |
|----------|--|-------|------------|-------------|--|------------------------|-------------|---------|---------|---|----------------------------------|------------|------|------------------|----------|
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | WOOD FIRED BOILERS (7) | WOOD | 175 | MMBTU/H | | Particulate Matter < 10 µ (PM10) | 3.97 | LB/H | | BACT-PSD |
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | WOOD FIRED BOILERS (7) | WOOD | 175 | MMBTU/H | | Nitrogen Oxides (NOx) | 27.89 | LB/H | | N/A |
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | WOOD FIRED BOILERS (7) | WOOD | 175 | MMBTU/H | | Carbon Monoxide | 31.8 | LB/H | | BACT-PSD |
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | WOOD FIRED BOILERS (7) | WOOD | 175 | MMBTU/H | | Sulfur Dioxide (SO2) | 22.13 | LB/H | | N/A |
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | WOOD HANDLING SYSTEM | | 130495 | ACFM | | Particulate Matter < 10 µ (PM10) | 6.71 | LB/H | | BACT-PSD |
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | AUXILIARY BOILER | FUEL OIL #2 | 227 | MMBTU/H | | Nitrogen Oxides (NOx) | 43.13 | LB/H | ON FUEL OIL | N/A |
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | AUXILIARY BOILER | FUEL OIL #2 | 227 | MMBTU/H | | Carbon Monoxide | 27.24 | LB/H | WITH FUEL OIL | BACT-PSD |
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | SEVEN BOILERS PURCHASED FROM AN ETHANOL PLANT. REBUILDING TO BURN WOOD AND TO GENERATE POWER, USING WOOD WASTE | AUXILIARY BOILER | FUEL OIL #2 | 227 | MMBTU/H | Oxidation catalyst, selective catalytic reduction, sodium bicarbonate injection, reverse air, baghouse w/98% control. | Particulate Matter < 10 µ (PM10) | 9.08 | LB/H | WITH FUEL OIL | BACT-PSD |
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | AUXILIARY BOILER | FUEL OIL #2 | 227 | MMBTU/H | | Sulfur Dioxide (SO2) | 2.84 | LB/H | FOR FUEL OIL | N/A |
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | AUXILIARY BOILER | NATURAL GAS | 247 | MMBTU/H | | Nitrogen Oxides (NOx) | 14.82 | LB/H | WITH NATURAL GAS | N/A |
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | AUXILIARY BOILER | NATURAL GAS | 247 | MMBTU/H | | Carbon Monoxide | 27.17 | LB/H | WITH NATURAL GAS | BACT-PSD |
| *OH-0269 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | AUXILIARY BOILER | NATURAL GAS | 247 | MMBTU/H | | Particulate Matter < 10 µ (PM10) | 1.73 | LB/H | WITH NATURAL GAS | BACT-PSD |

Northern Michigan University
RBLC

| RBLCID | FACILITY NAME | STATE | PERMIT No. | PERMIT DATE | DESCRIPTION | PROCESS NAME | FUEL | THRUPUT | UNIT | PROCESS NOTES | POLLUTANT | EMIS LIMIT | UNIT | AVG TIME | BASIS |
|----------|--|-------|------------|-------------|---|-------------------------------------|-------------|---------|--------------|--|----------------------------------|------------|----------|------------------|--------------------|
| *OH-0268 | BIOMASS ENERGY, LLC- SOUTH POINT POWER | OH | 07-00534 | 1/5/2004 | | AUXILIARY BOILER | NATURAL GAS | 247 | MMBTU/H | | Sulfur Dioxide (SO2) | 0.15 | LB/H | WITH NATURAL GAS | N/A |
| LA-0126 | JOYCE MILL | LA | PSD-LA-679 | 4/24/2002 | JOYCE MILL PRODUCES LUMBER AND WOOD WASTES, SUCH AS WOOD CHIPS, SHAVINGS, SAWDUST AND BARK. THE WOOD WASTE IS USED FOR FUEL IN THE BOILERS TO PRODUCE STEAM FOR THE MILL. | KIPPER BOILERS NO.1 AND NO.2 (EACH) | WOOD WASTE | 58.3 | MMBTU/H EACH | EMISSION POINTS 74A (NO.1) AND 74B (NO.2) | Carbon Monoxide | 105.5 | LB/H | EACH | Other Case-by-Case |
| LA-0126 | JOYCE MILL | LA | PSD-LA-679 | 4/24/2002 | | MCBURNAY BOILER NO.4 | WOOD WASTE | 154.2 | MMBTU/H | EMISSION POINT 76A. | Carbon Monoxide | 279.1 | LB/H | | Other Case-by-Case |
| VA-0268 | THERMAL VENTURES | VA | 30529 | 2/15/2002 | | BOILER, STEAM | WOOD | 120 | MMBTU/H | | Particulate Matter (PM) | 0.15 | LB/MMBTU | | Other Case-by-Case |
| VA-0268 | THERMAL VENTURES | VA | 30529 | 2/15/2002 | | BOILER, STEAM | WOOD | 120 | MMBTU/H | Wood limit 70% Mixture, Wood/Bark excluding any wood which contains chemical treatments or has affixed thereto paint and/or finishing materials or paper or plastic laminae; Average annual heat content: 5,000 Btu/lb HHV | Particulate Matter < 10 µ (PM10) | 0.14 | LB/MMBTU | | Other Case-by-Case |
| VA-0268 | THERMAL VENTURES | VA | 30529 | 2/15/2002 | | BOILER, STEAM | WOOD | 120 | MMBTU/H | | Sulfur Dioxide (SO2) | 0.47 | LB/MMBTU | | Other Case-by-Case |
| VA-0268 | THERMAL VENTURES | VA | 30529 | 2/15/2002 | STEAM PRODUCTION FACILITY | BOILER, STEAM | WOOD | 120 | MMBTU/H | | Nitrogen Dioxide (NO2) | 0.4 | LB/MMBTU | | Other Case-by-Case |
| VA-0268 | THERMAL VENTURES | VA | 30529 | 2/15/2002 | | BOILER, STEAM | WOOD | 120 | MMBTU/H | | Carbon Monoxide | 0.44 | LB/MMBTU | | Other Case-by-Case |
| VA-0268 | THERMAL VENTURES | VA | 30529 | 2/15/2002 | | BOILER, STEAM | COAL | 120 | MMBTU/H | In order to meet the annual emission limitations included in this permit, the wood/coal mixture shall not exceed 30% coal by BTU content on an annual basis. | Particulate Matter (PM) | 0.15 | LB/MMBTU | | Other Case-by-Case |

| RBLCID | FACILITY NAME | STATE | PERMIT No. | PERMIT DATE | DESCRIPTION | PROCESS NAME | FUEL | THRUPT | UNIT | PROCESS NOTES | POLLUTANT | EMIS LIMIT | UNIT | AVG TIME | BASIS |
|---------|-----------------------------|-------|------------------|-------------|---|--------------------------------|-------------|--------|---------|---|----------------------------------|------------|----------|----------|--------------------|
| VA-0268 | THERMAL VENTURES | VA | 30529 | 2/15/2002 | | BOILER, STEAM | COAL | 120 | MMBTU/H | Average annual heat content 13,000 Btu/lb HHV. Average sulfur content per shipment 0.9% and average ash content per shipment 7%. | Particulate Matter < 10 µ (PM10) | 0.14 | LB/MMBTU | | Other Case-by-Case |
| VA-0268 | THERMAL VENTURES | VA | 30529 | 2/15/2002 | | BOILER, STEAM | COAL | 120 | MMBTU/H | In order to meet the annual emission limitations included in this permit, the wood/coal mixture shall not exceed 30% coal by BTU content on an annual basis. Average annual heat content 13,000 Btu/lb HHV. Average sulfur content per shipment 0.8% and average ash content per shipment 7%. | Sulfur Dioxide (SO2) | 0.47 | LB/MMBTU | | Other Case-by-Case |
| VA-0268 | THERMAL VENTURES | VA | 30529 | 2/15/2002 | STEAM PRODUCTION FACILITY | BOILER, STEAM | COAL | 120 | MMBTU/H | | Nitrogen Oxides (NOx) | 0.4 | LB/MMBTU | | Other Case-by-Case |
| VA-0268 | THERMAL VENTURES | VA | 30529 | 2/15/2002 | | BOILER, STEAM | COAL | 120 | MMBTU/H | | Carbon Monoxide | 0.44 | LB/MMBTU | | Other Case-by-Case |
| LA-0125 | WILLAMETTE INDUSTRIES, INC. | LA | PSD-LA-627 (M-1) | 1/7/2002 | WILLAMETTE INDUSTRIES REQUESTED A PSD MODIFICATION TO INSTALL A REGENERATIVE THERMAL OXIDIZER OR CATALYTIC OXIDIZER (RTORCO), REMOVE THE PRODUCTION LIMIT IMPOSED BY PART 70 OPERATING PERMIT NO. 3249-0001/01/2 AND MODERNIZE THE PLYWOOD MANUFACTURING PROCESS AT THE DOODSON DIVISION. | WOOD FIRED BOILER | WOOD | 233 | MMBTU/H | EQ NO. 017. NO PHYSICAL MODIFICATION TO THE BOILERS WILL BE NEEDED (FIRING RATES WILL BE INCREASED) SO BACT IS NOT REQUIRED FOR EMISSIONS FROM BOILERS. | Nitrogen Oxides (NOx) | 47.91 | LB/H | | Other Case-by-Case |
| LA-0125 | WILLAMETTE INDUSTRIES, INC. | LA | PSD-LA-627 (M-1) | 1/7/2002 | | WOOD FIRED BOILER | WOOD | 233 | MMBTU/H | | Carbon Monoxide | 191.68 | LB/H | | Other Case-by-Case |
| LA-0125 | WILLAMETTE INDUSTRIES, INC. | LA | PSD-LA-627 (M-1) | 1/7/2002 | | VENNER DRYER NO.1 COOLING ZONE | NATURAL GAS | | | | Nitrogen Oxides (NOx) | 0.37 | LB/H | | BACT-PSD |
| LA-0125 | WILLAMETTE INDUSTRIES, INC. | LA | PSD-LA-627 (M-1) | 1/7/2002 | | VENNER DRYER NO.1 COOLING ZONE | NATURAL GAS | | | | Carbon Monoxide | 0.09 | LB/H | | BACT-PSD |
| LA-0125 | WILLAMETTE INDUSTRIES, INC. | LA | PSD-LA-627 (M-1) | 1/7/2002 | | VENNER DRYER NO.2 COOLING ZONE | NATURAL GAS | | | | Nitrogen Oxides (NOx) | 0.88 | LB/H | | BACT-PSD |
| LA-0125 | WILLAMETTE INDUSTRIES, INC. | LA | PSD-LA-627 (M-1) | 1/7/2002 | | VENNER DRYER NO.2 COOLING ZONE | NATURAL GAS | | | | Carbon Monoxide | 0.22 | LB/H | | BACT-PSD |
| LA-0125 | WILLAMETTE INDUSTRIES, INC. | LA | PSD-LA-627 (M-1) | 1/7/2002 | | VENNER DRYERS, HOT ZONES | NATURAL GAS | | | | Nitrogen Oxides (NOx) | 10.27 | LB/H | | BACT-PSD |
| LA-0125 | WILLAMETTE INDUSTRIES, INC. | LA | PSD-LA-627 (M-1) | 1/7/2002 | | VENNER DRYERS, HOT ZONES | NATURAL GAS | | | | Carbon Monoxide | 9.31 | LB/H | | BACT-PSD |

Northern Michigan University
RBLC

| RBLCD | FACILITY NAME | STATE | PERMIT No. | PERMIT DATE | DESCRIPTION | PROCESS NAME | FUEL | THRUPUT | UNIT | PROCESS NOTES | POLLUTANT | EMIS LIMIT | UNIT | AVG TIME | BASIS |
|---------|---------------------------------|-------|----------------------|-------------|--|---------------------------------------|---------------------|---------|------------------|--|----------------------------------|------------|----------|----------------|--------------------|
| VA-0267 | VPI POWER STATION | VA | 20124 | 8/30/2001 | | BOILER, OVERFEEED STOKER | COAL | 146.7 | MMBTU/H | | Particulate Matter < 10 µ (PM10) | 2.9 | LB/H | | BACT-PSD |
| VA-0267 | VPI POWER STATION | VA | 20124 | 8/30/2001 | | BOILER, OVERFEEED STOKER | COAL | 146.7 | MMBTU/H | | Sulfur Dioxide (SO2) | 23.6 | LB/H | | BACT-PSD |
| VA-0267 | VPI POWER STATION | VA | 20124 | 8/30/2001 | Steam generation for electricity. | BOILER, OVERFEEED STOKER | COAL | 146.7 | MMBTU/H | No. 11 boiler. Boiler produces steam for generation of electricity. | Nitrogen Dioxide (NO2) | 36.1 | LB/H | | BACT-PSD |
| VA-0267 | VPI POWER STATION | VA | 20124 | 8/30/2001 | | BOILER, OVERFEEED STOKER | COAL | 146.7 | MMBTU/H | | Carbon Monoxide | 33.2 | LB/H | | BACT-PSD |
| VA-0267 | VPI POWER STATION | VA | 20124 | 8/30/2001 | | BOILER, OVERFEEED STOKER | COAL | 146.7 | MMBTU/H | | Particulate Matter (PM) | 2.9 | LB/H | | BACT-PSD |
| AR-0045 | COLUMBIAN CHEMICALS - EL DORADO | AR | 906-AOP-R1 (70-0014) | 8/9/2001 | This plant makes carbon black using the oil furnace process. This determination is a modification. Emission increases of SO2 and NOX will exceed the PSD significance levels. Emissions are less than the PSD threshold. Other pollutants proposed are lower than the past actual emissions because of the addition of new control equipment. Carbon Disulfide 87.76 Carbonyl sulfide 13.46 Hydrogen 117.75 TRS 219.04 | COAL-FIRED BOILERS (2) | SUB-BITUMINOUS COAL | 9700 | MMBTU/H FOR EACH | CO catalyst technology used with a coal fired source was deemed technically infeasible. Due to position in ductwork, the catalyst is exposed to a substantial amount of fly ash in the flue gas stream. No physical modification was made for this process under this determination, but permitted emission rates for ppm emissions of CO change due to the use of new emission factors. | Carbon Monoxide | 100 | PPM | 24 hr. average | Other Case-by-Case |
| AR-0045 | COLUMBIAN CHEMICALS - EL DORADO | AR | 906-AOP-R1 (70-0014) | 8/9/2001 | | CARBON BLACK MFG, UNIT D STACK & VENT | NATURAL GAS | | | | Sulfur Dioxide (SO2) | 0.2 | LB/H | | BACT-PSD |
| AR-0045 | COLUMBIAN CHEMICALS - EL DORADO | AR | 906-AOP-R1 (70-0014) | 8/9/2001 | | CARBON BLACK MFG, UNIT D STACK & VENT | NATURAL GAS | | | | Nitrogen Oxides (NOx) | 7.7 | LB/H | | BACT-PSD |
| AR-0045 | COLUMBIAN CHEMICALS - EL DORADO | AR | 906-AOP-R1 (70-0014) | 8/9/2001 | | CARBON BLACK MFG., UNITS A, B, & C | FEEDSTOCK OIL | | | Throughput to confidential. This carbon black mfg process is being added. New stacks: SN-31, SN-48, SN-49. BACT determination for SO2 and NOx only. | Sulfur Dioxide (SO2) | 2630 | LB/H | combined | BACT-PSD |
| AR-0045 | COLUMBIAN CHEMICALS - EL DORADO | AR | 906-AOP-R1 (70-0014) | 8/9/2001 | | CARBON BLACK MFG., UNITS A, B, & C | FEEDSTOCK OIL | | | | Nitrogen Oxides (NOx) | 246 | LB/H | combined | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | BOILER, POWER, COAL-FIRED | COAL | 249 | MMBTU/H | | Particulate Matter (PM) | 0.16 | LB/MMBTU | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | MODIFICATION FOR INSTALLATION OF NEW EQUIPMENT TO INCREASE PRODUCTION CAPACITY. | BOILER, POWER, COAL-FIRED | COAL | 249 | MMBTU/H | | Sulfur Dioxide (SO2) | 0.8 | LB/MMBTU | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | BOILER, POWER, COAL-FIRED | COAL | 249 | MMBTU/H | | Nitrogen Oxides (NOx) | 0.4 | LB/MMBTU | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | BOILER, POWER, COAL-FIRED | COAL | 249 | MMBTU/H | | Carbon Monoxide | 0.208 | LB/MMBTU | | BACT-PSD |

Northern Michigan University
RBLC

| REC'D | FACILITY NAME | STATE | PERMIT NO. | PERMIT DATE | DESCRIPTION | PROCESS NAME | FUEL | THRUPUT | UNIT | PROCESS NOTES | POLLUTANT | EMIS LIMIT | UNIT | AVG TIME | BASIS |
|---------|-----------------|-------|------------|-------------|---|--------------------------------|----------------|---------|----------|--|-------------------------|------------|-----------------|----------|----------|
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | BOILER, POWER, OIL-FIRED | NO. 6 FUEL OIL | 249 | MMBTU/H | | Particulate Matter (PM) | 0.0562 | LB/MMBTU | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | BOILER, POWER, OIL-FIRED | NO. 6 FUEL OIL | 249 | MMBTU/H | | Sulfur Dioxide (SO2) | 0.8 | LB/MMBTU | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | BOILER, POWER, OIL-FIRED | NO. 6 FUEL OIL | 249 | MMBTU/H | | Nitrogen Oxides (NOx) | 0.367 | LB/MMBTU | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | BOILER, POWER, OIL-FIRED | NO. 6 FUEL OIL | 249 | MMBTU/H | | Carbon Monoxide | 0.033 | LB/MMBTU | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | BOILER, POWER, WOODWASTE-FIRED | WOODWASTE | 600 | MMBTU/H | POWER BOILER CAN FIRE COAL, NO. 6 FUEL OIL, OR BARK/WOOD FIBER SLUDGE. | Particulate Matter (PM) | 0.25 | LB/MMBTU | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | BOILER, POWER, WOODWASTE-FIRED | WOODWASTE | 600 | MMBTU/H | | Sulfur Dioxide (SO2) | 0.024 | LB/MMBTU | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | BOILER, POWER, WOODWASTE-FIRED | WOODWASTE | 600 | MMBTU/H | | Nitrogen Oxides (NOx) | 0.36 | LB/MMBTU | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | BOILER, POWER, WOODWASTE-FIRED | WOODWASTE | 600 | MMBTU/H | | Carbon Monoxide | 0.5 | LB/MMBTU | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | MODIFICATION FOR INSTALLATION OF NEW EQUIPMENT TO INCREASE PRODUCTION CAPACITY. | RECOVERY BOILER | NO. 6 FUEL OIL | 557 | MMBTU/H | | Sulfur Dioxide (SO2) | 979.2 | LB/H | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | RECOVERY BOILER | NO. 6 FUEL OIL | 557 | MMBTU/H | | Nitrogen Dioxide (NO2) | 666.5 | LB/H | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | RECOVERY BOILER | NO. 6 FUEL OIL | 557 | MMBTU/H | | Carbon Monoxide | 357.1 | LB/H | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | RECOVERY BOILER | NO. 6 FUEL OIL | 557 | MMBTU/H | BOILER FIRES AN AVERAGE OF 6.69 MILLION POUNDS OF BLACK LIQUOR SOLIDS PER DAY. | Particulate Matter (PM) | 0.044 | GRDSCF @ 8% O2 | | N/A |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | SMELT TANKS | | | | | Sulfur Dioxide (SO2) | 6.2 | LB/H | | BACT-PSD |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | LIME KILN | NO. 6 FUEL OIL | 212 | LB/MMBTU | | Particulate Matter (PM) | 0.13 | GRDSCF @ 10% O2 | | N/A |
| NC-0092 | RIEGELWOOD MILL | NC | 03138R16 | 5/10/2001 | | LIME KILN | NO. 6 FUEL OIL | 212 | LB/MMBTU | | Total Reduced Sulfur | 8 | PPM @ 10% O2 | | N/A |



APPENDIX E
ESA Documentation



STATE OF MICHIGAN

DEPARTMENT OF NATURAL RESOURCES
LANSING

JENNIFER M. GRANHOLM
GOVERNOR

REBECCA A. HUMPHRIES
DIRECTOR

August 8, 2006

Mr. Jeffrey Jaros
NTH Consultants, Ltd.
608 S. Washington
Lansing, MI 48933

RE: Two proposed air permit locations in Holland and Marquette, Michigan submitted to DNR Endangered Species Assessment web application

Dear Mr. Jaros:

The location of the proposed projects were checked against known localities for rare species and unique natural features, which are recorded in a statewide database. This continuously updated database is a comprehensive source of existing data on Michigan's endangered, threatened, or otherwise significant plant and animal species, natural plant communities, and other natural features. Records in the database indicate that a qualified observer has documented the presence of special natural features at a site. The absence of records in the database for a particular site may mean that the site has not been surveyed. Records are not always up-to-date, and may require verification. In some cases, the only way to obtain a definitive statement on the status of natural features is to have a competent biologist perform a complete field survey.

Under Act 451 of 1994, the Natural Resources and Environmental Protection Act, Part 365, Endangered Species Protection, "a person shall not take, possess, transport, ...fish, plants, and wildlife indigenous to the state and determined to be endangered or threatened," unless first receiving an Endangered Species Permit from the Department of Natural Resources, Wildlife Division. *Responsibility to protect endangered and threatened species is not limited to the list below. Other species may be present that have not been recorded in the database.*

The presence of threatened or endangered species does not preclude activities or development, but may require alterations in the project plan. Special concern species are not protected under endangered species legislation, but recommendations regarding their protection may be provided. Protection of special concern species will help prevent them from declining to the point of being listed as threatened or endangered in the future.

The following is a summary of the results for the project in Ottawa County, City of Holland, T5N R16W section 36 and Marquette County, City of Marquette, T48N R25W section 11:

The project should have no impact on rare or unique natural features at the location specified above if it proceeds according to the plans provided. Please contact me for an evaluation if the project plans are changed.

Thank you in for your coordination in addressing the protection of Michigan's natural resource heritage. Responses and correspondence can be sent to: Michigan Department of Natural Resources, Wildlife Division -- Natural Heritage Program, PO Box 30180, Lansing, MI 48909. If you have further questions, please call me at 517-373-1263 or e-mail at SargenL2@michigan.gov.

Sincerely,

Lori G. Sargent
Endangered Species Specialist
Wildlife Division



United States Department of the Interior

FISH AND WILDLIFE SERVICE
East Lansing Field Office (ES)
2651 Coolidge Road, Suite 101
East Lansing, Michigan 48823-6316

IN REPLY REFER TO:

November 24, 2006

Mr. Jeffrey P. Jaros
NTH Consultants, Ltd.
608 S. Washington Avenue
Lansing, MI 48933

Re: Endangered Species List Request, Proposed Construction of Solid Fuel Fired Boiler,
Northern Michigan University, Marquette, Marquette County, Michigan

Dear Mr. Jaros:

Thank you for your October 24, 2006 request for information regarding federally listed and proposed threatened and endangered species, candidate species, or critical habitat near your proposed project. Your request and this response are made pursuant to the Endangered Species Act of 1973, as amended (Act). Under this project, Northern Michigan University proposes to install a cogeneration of coal/wood/natural gas fired circulating fluidized bed boiler on the north end of its campus, next to the existing Ripley Heating Plant.

Our records do not indicate the presence of federally listed species or critical habitat near your proposed project. This precludes the need for further action on this project as required by the Act. If, however, more than six months pass, project plans change, or new information becomes available that indicates listed species or proposed species may be affected, you should conduct further consultation with this office.

We appreciate your concern for endangered and threatened species. Any questions can be directed to Tameka Dandridge of this office at Tameka_Dandridge@fws.gov or 517/351-8315.

Sincerely,

Craig A. Czarniecki
Field Supervisor

cc: MDNR-Wildlife Division, Lansing, MI (Attn: Lori Sargent)

s: admin/archives/nov06/se list/NTH-NMU~solidfuel.tnd.doc



APPENDIX F

Cooling Tower Modeling Output

prep

 EPRI PLUME AND DRIFT ANALYSIS SYSTEM PREPROCESSOR CODE, PRE-RELEASE VERSION 09-01-90
 CASE STUDY: Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

INPUT INFORMATION

 SURFACE TAPE TYPE: CD144
 TOWER TYPE: LINEAR MECHANICAL DRAFT
 TOWER HEIGHT (M): 12.50
 TOWER DIAMETER (M): 47.03
 TOWER HEAT (KW): 7000.00
 TOWER AIR FLOW (KG/S): 679.50
 SITE LATITUDE: 46.60
 SITE LONGITUDE: 87.40
 SITE TIME ZONE: EASTERN
 ROUGHNESS HEIGHT (CM): 0.07
 REFERENCE HEIGHT (M): 10.00
 RECORD STOPPING SWITCH: 8760
 RECORD SKIPPING FACTOR: 1
 HOURLY RECORD PRINT LOG: NOT SELECTED
 BI-DAILY MIXING HEIGHT TAPE: SELECTED
 MIXING HEIGHT TYPE: RURAL
 FOGGING/ICING OPTION: SELECTED
 DRIFT OPTION: SELECTED

MONTHLY CLEARNESS INDEX

 JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
 --- --- --- --- --- --- --- --- --- --- --- ---
 .460 .490 .520 .490 .530 .550 .560 .550 .530 .500 .420 .420

TOTAL DAILY SOLAR ENERGY DEPOSITION (LONG-TERM AVERAGE FOR MONTH)

 JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
 --- --- --- --- --- --- --- --- --- --- --- ---
 5.74 8.79 13.10 16.08 20.47 22.69 22.52 19.34 14.78 10.05 5.82

4.60

1

*****WIND SPEED FREQUENCY

TABLE*****

Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

*****WIND

FROM*****
 SPEED N NNE NE ENE E ESE SE SSE S SSW SW WSW W
 WNW NW NNW
 RANGE *****WIND
 HEADED*****
 (M/S) S SSW SW WSW W WNW NW NNW N NNE NE ENE E
 ESE SE SSE SUM

0 TO 1 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
 0.000 0.000 0.000 0.000
 1 TO 2 0.009 0.003 0.003 0.003 0.004 0.002 0.003 0.004 0.008 0.009 0.008 0.005 0.007
 0.003 0.004 0.005 0.081

prep

| | | | | | | | | | | | | | | | |
|-------|----|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 2 | TO | 3 | 0.017 | 0.009 | 0.011 | 0.007 | 0.009 | 0.004 | 0.007 | 0.010 | 0.022 | 0.017 | 0.012 | 0.015 | 0.022 |
| 0.011 | | | 0.009 | 0.010 | 0.192 | | | | | | | | | | |
| 3 | TO | 4 | 0.016 | 0.015 | 0.012 | 0.006 | 0.007 | 0.003 | 0.006 | 0.012 | 0.026 | 0.021 | 0.015 | 0.007 | 0.019 |
| 0.013 | | | 0.015 | 0.009 | 0.202 | | | | | | | | | | |
| 4 | TO | 5 | 0.014 | 0.019 | 0.015 | 0.005 | 0.002 | 0.002 | 0.007 | 0.010 | 0.031 | 0.016 | 0.013 | 0.008 | 0.011 |
| 0.012 | | | 0.011 | 0.008 | 0.183 | | | | | | | | | | |
| 5 | TO | 6 | 0.012 | 0.012 | 0.010 | 0.002 | 0.001 | 0.001 | 0.006 | 0.008 | 0.030 | 0.016 | 0.007 | 0.007 | 0.006 |
| 0.006 | | | 0.007 | 0.008 | 0.139 | | | | | | | | | | |
| 6 | TO | 7 | 0.012 | 0.006 | 0.004 | 0.001 | 0.000 | 0.001 | 0.002 | 0.005 | 0.017 | 0.007 | 0.004 | 0.003 | 0.004 |
| 0.004 | | | 0.006 | 0.005 | 0.083 | | | | | | | | | | |
| 7 | TO | 8 | 0.008 | 0.006 | 0.001 | 0.000 | 0.000 | 0.000 | 0.001 | 0.003 | 0.013 | 0.006 | 0.002 | 0.002 | 0.002 |
| 0.003 | | | 0.005 | 0.002 | 0.056 | | | | | | | | | | |
| 8 | TO | 9 | 0.005 | 0.003 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.005 | 0.003 | 0.002 | 0.001 | 0.001 |
| 0.001 | | | 0.002 | 0.002 | 0.025 | | | | | | | | | | |
| 9 | TO | 10 | 0.006 | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.003 | 0.003 | 0.001 | 0.001 | 0.001 |
| 0.000 | | | 0.002 | 0.001 | 0.019 | | | | | | | | | | |
| 10 | TO | 11 | 0.005 | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | | | 0.000 | 0.000 | 0.011 | | | | | | | | | | |
| 11 | TO | 12 | 0.002 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | | | 0.000 | 0.000 | 0.005 | | | | | | | | | | |
| 12 | TO | 13 | 0.001 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | | | 0.000 | 0.000 | 0.003 | | | | | | | | | | |
| 13 | TO | 14 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | | | 0.000 | 0.000 | 0.001 | | | | | | | | | | |
| 14 | TO | 15 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | | | 0.000 | 0.000 | 0.001 | | | | | | | | | | |
| 15 | TO | 20 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | | | 0.000 | 0.000 | 0.000 | | | | | | | | | | |
| 20 | TO | 25 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | | | 0.000 | 0.000 | 0.000 | | | | | | | | | | |
| 25 | TO | 30 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | | | 0.000 | 0.000 | 0.000 | | | | | | | | | | |
| 30 | TO | OVER | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | | | 0.000 | 0.000 | 0.000 | | | | | | | | | | |

 AVERAGE 4.47699 VARIANCE 4.52228 STD DEV 2.12657
 STD ERR 0.02459 SKEWNESS 1.31718 KURTOSIS 2.01213

 1 *****RELATIVE HUMIDITY FREQUENCY

TABLE*****

Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

| RELATIVE HUMIDITY RANGE (%) | *****WIND | | | | | | | | | | | | | | |
|-----------------------------|-----------|-------|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--|
| FROM | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | W | |
| WIND | NW | NNW | *****WIND | | | | | | | | | | | | |
| HEADED | S | SSW | SW | WSW | W | NNW | NW | NNW | N | NNE | NE | ENE | E | | |
| ESE | SE | SSE | SUM | | | | | | | | | | | | |
| 0 TO 10 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 10 TO 20 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.003 | | | | | | | | | | | | |
| 20 TO 30 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 | 0.001 | 0.002 | 0.003 | 0.003 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | |
| 0.000 | 0.000 | 0.000 | 0.015 | | | | | | | | | | | | |
| 30 TO 40 | 0.001 | 0.003 | 0.004 | 0.002 | 0.002 | 0.002 | 0.004 | 0.005 | 0.007 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | |
| 0.003 | 0.001 | 0.001 | 0.050 | | | | | | | | | | | | |
| 40 TO 50 | 0.002 | 0.005 | 0.007 | 0.002 | 0.001 | 0.000 | 0.002 | 0.005 | 0.013 | 0.007 | 0.007 | 0.004 | 0.005 | 0.005 | |
| 0.003 | 0.002 | 0.002 | 0.066 | | | | | | | | | | | | |
| 50 TO 60 | 0.008 | 0.008 | 0.008 | 0.004 | 0.001 | 0.001 | 0.001 | 0.005 | 0.020 | 0.011 | 0.008 | 0.006 | 0.008 | 0.008 | |
| 0.005 | 0.005 | 0.004 | 0.103 | | | | | | | | | | | | |

prep

60 TO 70 0.014 0.010 0.009 0.003 0.003 0.001 0.002 0.007 0.018 0.012 0.008 0.007 0.010
0.009 0.011 0.006 0.130
70 TO 80 0.015 0.012 0.008 0.003 0.002 0.001 0.003 0.006 0.026 0.016 0.009 0.010 0.014
0.014 0.013 0.012 0.162
80 TO 90 0.029 0.014 0.009 0.006 0.006 0.003 0.005 0.009 0.026 0.020 0.016 0.010 0.022
0.014 0.018 0.014 0.221
90 TO 100 0.027 0.016 0.009 0.004 0.004 0.004 0.007 0.009 0.029 0.020 0.009 0.007 0.007
0.005 0.010 0.009 0.175
100 TO OVER 0.012 0.009 0.003 0.002 0.002 0.001 0.004 0.005 0.011 0.008 0.004 0.002 0.003
0.001 0.003 0.003 0.074

AVERAGE 74.66025 VARIANCE 402.23911 STD DEV 20.05590
STD ERR 0.23196 SKEWNESS 1.08593 KURTOSIS 1.22048

1 *****DEW POINT TEMPERATURE FREQUENCY

TABLE*****
Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

DEW POINT *****WIND
FROM*****
TEMP N NNE NE ENE E ESE SE SSE S SSW SW WSW W
WNW NW NNW
RANGE (C) *****WIND
HEADED*****
S SSW SW WSW W WNW NW NNW N NNE NE ENE E
ESE SE SSE SUM

-45 TO -40 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
0.000 0.000 0.000 0.000
-40 TO -35 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
0.000 0.000 0.000 0.000
-35 TO -30 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.001
0.000 0.000 0.000 0.001
-30 TO -25 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.001 0.002 0.001 0.004
0.002 0.000 0.000 0.010
-25 TO -20 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.001 0.000 0.000 0.002 0.003
0.001 0.001 0.001 0.010
-20 TO -15 0.001 0.000 0.001 0.000 0.001 0.001 0.000 0.000 0.003 0.004 0.004 0.005 0.009
0.006 0.008 0.004 0.047
-15 TO -10 0.016 0.007 0.003 0.001 0.002 0.002 0.004 0.003 0.005 0.011 0.008 0.006 0.011
0.008 0.015 0.010 0.111
-10 TO -5 0.016 0.012 0.008 0.003 0.001 0.002 0.007 0.007 0.013 0.007 0.005 0.003 0.005
0.006 0.008 0.005 0.108
-5 TO 0 0.021 0.015 0.009 0.004 0.005 0.005 0.005 0.007 0.025 0.014 0.011 0.006 0.009
0.006 0.008 0.007 0.158
0 TO 5 0.018 0.014 0.008 0.004 0.003 0.001 0.004 0.007 0.019 0.012 0.004 0.003 0.009
0.007 0.010 0.012 0.138
5 TO 10 0.021 0.015 0.013 0.004 0.004 0.002 0.004 0.010 0.024 0.013 0.007 0.007 0.008
0.006 0.006 0.007 0.150
10 TO 15 0.014 0.010 0.012 0.004 0.003 0.001 0.004 0.012 0.030 0.014 0.011 0.008 0.012
0.009 0.004 0.003 0.151
15 TO 20 0.003 0.004 0.003 0.003 0.002 0.001 0.002 0.007 0.033 0.021 0.012 0.007 0.003
0.002 0.002 0.001 0.106
20 TO 25 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.003 0.002 0.001 0.001 0.001
0.001 0.000 0.000 0.010
25 TO 30 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
0.000 0.000 0.000 0.000
30 TO 35 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
0.000 0.000 0.000 0.000
35 TO 40 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
0.000 0.000 0.000 0.000
40 TO 45 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
0.000 0.000 0.000 0.000

prep

45 TO OVER 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
0.000 0.000 0.000 0.000

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AVERAGE    1.50883    VARIANCE 120.84354    STD DEV   10.99289
STD ERR     0.12714    SKEWNESS  0.12920     KURTOSIS  2.21745

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1 ***** DRY BULB TEMPERATURE FREQUENCY
TABLE*****

Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

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DRY BULB ***** WIND
FROM*****
TEMP      N    NNE  NE   ENE   E   ESE  SE   SSE  S   SSW  SW   WSW  W
WNW  NW  NNW
RANGE (C) ***** WIND
HEADED*****
          S    SSW  SW   WSW  W   WNW  NW  NNW  N   NNE  NE   ENE  E
ESE  SE   SSE  SUM

```

| | | | | | | | | | | | | | | | |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| -45 TO -40 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 TO -35 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| -35 TO -30 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| -30 TO -25 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| -25 TO -20 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.002 | 0.001 | 0.003 | 0.002 |
| -20 TO -15 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.001 | 0.002 | 0.003 | 0.006 | 0.003 |
| -15 TO -10 | 0.004 | 0.002 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.004 | 0.007 | 0.004 | 0.005 | 0.013 | 0.006 |
| -10 TO -5 | 0.017 | 0.008 | 0.006 | 0.003 | 0.001 | 0.001 | 0.003 | 0.004 | 0.008 | 0.011 | 0.009 | 0.006 | 0.007 | 0.008 | 0.008 |
| -5 TO 0 | 0.023 | 0.013 | 0.008 | 0.002 | 0.003 | 0.004 | 0.005 | 0.005 | 0.012 | 0.009 | 0.007 | 0.003 | 0.006 | 0.006 | 0.006 |
| 0 TO 5 | 0.020 | 0.017 | 0.007 | 0.005 | 0.005 | 0.002 | 0.005 | 0.005 | 0.020 | 0.013 | 0.007 | 0.005 | 0.010 | 0.008 | 0.012 |
| 5 TO 10 | 0.012 | 0.010 | 0.006 | 0.002 | 0.002 | 0.001 | 0.004 | 0.005 | 0.018 | 0.007 | 0.004 | 0.004 | 0.007 | 0.003 | 0.003 |
| 10 TO 15 | 0.017 | 0.011 | 0.009 | 0.003 | 0.003 | 0.002 | 0.005 | 0.009 | 0.025 | 0.015 | 0.004 | 0.004 | 0.006 | 0.005 | 0.005 |
| 15 TO 20 | 0.011 | 0.008 | 0.009 | 0.003 | 0.003 | 0.001 | 0.003 | 0.008 | 0.025 | 0.012 | 0.008 | 0.005 | 0.005 | 0.005 | 0.005 |
| 20 TO 25 | 0.004 | 0.008 | 0.011 | 0.005 | 0.003 | 0.001 | 0.003 | 0.012 | 0.029 | 0.013 | 0.010 | 0.008 | 0.008 | 0.006 | 0.006 |
| 25 TO 30 | 0.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.000 | 0.001 | 0.002 | 0.009 | 0.007 | 0.005 | 0.003 | 0.003 | 0.002 | 0.002 |
| 30 TO 35 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.003 | 0.003 | 0.003 | 0.002 | 0.001 | 0.000 | 0.000 |
| 35 TO 40 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40 TO 45 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45 TO OVER | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

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AVERAGE    6.44997    VARIANCE 154.27522    STD DEV   12.42076
STD ERR     0.14365    SKEWNESS  1.16754     KURTOSIS  2.32720

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prep

1 *****STABILITY CLASS FREQUENCY
TABLE*****

Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

STABILITY *****WIND
FROM*****
CLASS N NNE NE ENE E ESE SE SSE S SSW SW WSW W
WNW NW NNW *****WIND

| HEADED***** | | S | SSW | SW | WSW | W | WNW | NW | NNW | N | NNE | NE | ENE | E |
|-------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| ESE | SE | SSE | SUM | | | | | | | | | | | |
| | 1 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.002 | | | | | | | | | | | |
| | 2 | 0.003 | 0.003 | 0.004 | 0.003 | 0.002 | 0.002 | 0.002 | 0.003 | 0.003 | 0.003 | 0.002 | 0.002 | 0.003 |
| 0.001 | 0.001 | 0.001 | 0.037 | | | | | | | | | | | |
| | 3 | 0.007 | 0.011 | 0.016 | 0.005 | 0.002 | 0.001 | 0.003 | 0.005 | 0.016 | 0.009 | 0.009 | 0.008 | 0.007 |
| 0.005 | 0.004 | 0.003 | 0.113 | | | | | | | | | | | |
| | 4 | 0.072 | 0.053 | 0.028 | 0.010 | 0.010 | 0.006 | 0.017 | 0.029 | 0.085 | 0.049 | 0.029 | 0.024 | 0.032 |
| 0.030 | 0.041 | 0.030 | 0.545 | | | | | | | | | | | |
| | 5 | 0.015 | 0.007 | 0.007 | 0.005 | 0.006 | 0.004 | 0.006 | 0.011 | 0.035 | 0.019 | 0.012 | 0.009 | 0.014 |
| 0.011 | 0.011 | 0.009 | 0.180 | | | | | | | | | | | |
| | 6 | 0.009 | 0.002 | 0.002 | 0.001 | 0.002 | 0.001 | 0.002 | 0.004 | 0.014 | 0.015 | 0.009 | 0.005 | 0.016 |
| 0.006 | 0.005 | 0.006 | 0.102 | | | | | | | | | | | |
| | 7 | 0.003 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.003 | 0.002 | 0.003 | 0.002 | 0.003 |
| 0.001 | 0.001 | 0.001 | 0.021 | | | | | | | | | | | |

| | | | | | |
|---------|---------|----------|---------|----------|---------|
| AVERAGE | 4.25201 | VARIANCE | 0.99227 | STD DEV | 0.99613 |
| STD ERR | 0.01152 | SKENNESS | 1.07871 | KURTOSIS | 1.21936 |

1 *****K FREQUENCY
TABLE*****

Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

K *****WIND
FROM*****
(UA/VE) N NNE NE ENE E ESE SE SSE S SSW SW WSW W
WNW NW NNW *****WIND

| RANGE | | S | SSW | SW | WSW | W | WNW | NW | NNW | N | NNE | NE | ENE | E |
|-------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| ESE | SE | SSE | SUM | | | | | | | | | | | |
| 0.0 | TO 0.1 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | |
| 0.1 | TO 0.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | |
| 0.2 | TO 0.3 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | |
| 0.3 | TO 0.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | |
| 0.4 | TO 0.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | |
| 0.5 | TO 0.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | |
| 0.6 | TO 0.7 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | |
| 0.7 | TO 0.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | |
| 0.8 | TO 0.9 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

prep

| | | | | | | | | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.9 | TO | 1.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.0 | TO | 1.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.2 | TO | 1.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.4 | TO | 1.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.6 | TO | 1.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.8 | TO | 2.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.0 | TO | 2.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.5 | TO | 3.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.0 | TO | OVER | 0.110 | 0.078 | 0.058 | 0.024 | 0.022 | 0.014 | 0.031 | 0.054 | 0.155 | 0.098 | 0.064 | 0.050 | 0.075 |
| 0.054 | 0.062 | 0.051 | 1.000 | | | | | | | | | | | | |

```
*****
*****
AVERAGE      3.50000      VARIANCE      0.00000      STD DEV       0.00000
STD ERR       0.00000      SKEWNESS      1.00000      KURTOSIS     1.00000
*****
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*****
*****
1 *****VSTAR FREQUENCY
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TABLE*****
Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)
*****WIND
```

| FROM | VSTAR | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | |
|--------|-------|-------|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| WNW | NW | NNW | *****WIND | | | | | | | | | | | | |
| RANGE | | ***** | | | | | | | | | | | | | |
| HEADED | | S | SSW | SW | WSW | W | WNW | NW | NNW | N | NNE | NE | ENE | E | |
| ESE | SE | SSE | SUM | | | | | | | | | | | | |
| 0 | TO | 1 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 1 | TO | 2 | 0.093 | 0.067 | 0.054 | 0.023 | 0.020 | 0.011 | 0.026 | 0.048 | 0.141 | 0.087 | 0.058 | 0.047 | 0.070 |
| 0.052 | 0.056 | 0.045 | 0.895 | | | | | | | | | | | | |
| 2 | TO | 3 | 0.003 | 0.002 | 0.001 | 0.000 | 0.000 | 0.001 | 0.001 | 0.000 | 0.002 | 0.002 | 0.001 | 0.001 | 0.001 |
| 0.001 | 0.001 | 0.002 | 0.020 | | | | | | | | | | | | |
| 3 | TO | 4 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.004 | | | | | | | | | | | | |
| 4 | TO | 5 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 | 0.001 |
| 0.000 | 0.001 | 0.001 | 0.007 | | | | | | | | | | | | |
| 5 | TO | 6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 6 | TO | 7 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 7 | TO | 8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 8 | TO | 9 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 9 | TO | 10 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 10 | TO | 11 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 11 | TO | 12 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 12 | TO | 13 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 13 | TO | 14 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

prep

0.000 0.000 0.000 0.000
 14 TO 15 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
 0.000 0.000 0.000 0.000
 15 TO 20 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
 0.000 0.000 0.000 0.000
 20 TO 25 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
 0.000 0.000 0.000 0.000
 25 TO 30 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
 0.000 0.000 0.000 0.000
 30 TO OVER 0.012 0.009 0.003 0.002 0.002 0.001 0.004 0.005 0.011 0.008 0.004 0.002 0.003
 0.001 0.003 0.003 0.074

 AVERAGE 4.03170 VARIANCE 76.75311 STD DEV 8.76089
 STD ERR 0.10132 SKEWNESS 3.54087 KURTOSIS 12.83027

 1 *****PLUME LENGTH PARAMETER FREQUENCY
 TABLE*****
 Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

| PLUME | | *****WIND | | | | | | | | | | | | | |
|-------------------------|---|-----------|-----------|-----|-----|---|-----|----|-----|---|-----|----|-----|---|--|
| FROM* | ***** | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | |
| LENGTH | ***** | | | | | | | | | | | | | | |
| WNW | NW | NNW | *****WIND | | | | | | | | | | | | |
| RANGE (M) | ***** | S | SSW | SW | WSW | W | WNW | NW | NNW | N | NNE | NE | ENE | E | |
| HEADED* | ***** | ESE | SE | SSE | SUM | | | | | | | | | | |
| 0.0 TO 0.2 | 0.099 0.071 0.054 0.023 0.020 0.012 0.027 0.049 0.145 0.091 0.060 0.048 0.072 | | | | | | | | | | | | | | |
| 0.053 0.059 0.047 0.931 | | | | | | | | | | | | | | | |
| 0.2 TO 0.4 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 0.4 TO 0.6 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 0.6 TO 0.8 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 0.8 TO 1.0 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 1.0 TO 1.2 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 1.2 TO 1.4 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 1.4 TO 1.6 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 1.6 TO 1.8 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 1.8 TO 2.0 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 2.0 TO 2.2 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 2.2 TO 2.4 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 2.4 TO 2.6 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 2.6 TO 2.8 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 2.8 TO 3.0 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 3.0 TO 3.2 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 3.2 TO 3.4 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |
| 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | | |
| 3.4 TO 3.6 | 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | | | | | | | | |

prep
 Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

| PLUME | | *****WIND | | | | | | | | | | | | | |
|--------------|--------|-----------|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--|
| FROM | LENGTH | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | |
| WNW | NW | NNW | *****WIND | | | | | | | | | | | | |
| RANGE (M) | HEADED | S | SSW | SW | WSW | W | WNW | NW | NNW | N | NNE | NE | ENE | E | |
| ESE | SE | SSE | SUM | | | | | | | | | | | | |
| 10.0 TO 10.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 10.4 TO 10.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 10.8 TO 11.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 11.2 TO 11.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 11.6 TO 12.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 12.0 TO 12.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 12.4 TO 12.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 12.8 TO 13.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 13.2 TO 13.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 13.6 TO 14.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 14.0 TO 14.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 14.4 TO 14.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 14.8 TO 15.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 15.2 TO 15.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 15.6 TO 16.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 16.0 TO 16.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.002 | | | | | | | | | | | | |
| 16.4 TO 16.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 16.8 TO 17.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 17.2 TO 17.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.000 | | | | | | | | | | | | |
| 17.6 TO 18.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.001 | 0.000 | 0.003 | | | | | | | | | | | | |
| 18.0 TO 18.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 18.4 TO 18.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 18.8 TO 19.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 19.2 TO 19.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.001 | | | | | | | | | | | | |
| 19.6 TO 20.0 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.001 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.004 | | | | | | | | | | | | |
| 20.0 TO 21.0 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.003 | | | | | | | | | | | | |
| 21.0 TO 22.0 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.004 | | | | | | | | | | | | |
| 22.0 TO 23.0 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.001 | 0.001 | 0.000 | 0.000 | |
| 0.000 | 0.000 | 0.000 | 0.004 | | | | | | | | | | | | |
| 23.0 TO 24.0 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 | |

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| | | | | | | | | | | | | | | | |
|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 3.9 TO 4.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.0 TO 4.1 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.1 TO 4.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.2 TO 4.3 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.3 TO 4.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.4 TO 4.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.5 TO 4.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.6 TO 4.7 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.7 TO 4.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.8 TO 4.9 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.9 TO 5.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

1 *****PLUME HEIGHT PARAMETER FREQUENCY
 TABLE*****

Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

| PLUME | | *****WIND | | | | | | | | | | | | | | |
|-------------|-------|-----------|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| FROM***** | | ***** | | | | | | | | | | | | | | |
| HEIGHT | | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | | |
| WNW | NW | NNW | *****WIND | | | | | | | | | | | | | |
| RANGE (M) | ***** | | | | | | | | | | | | | | | |
| HEADED***** | | ***** | | | | | | | | | | | | | | |
| ESE | SE | SSE | SUM | S | SSW | SW | WSW | W | WNW | NW | NNW | N | NNE | NE | ENE | E |
| 5.0 TO 5.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.2 TO 5.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.4 TO 5.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.6 TO 5.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.8 TO 6.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.0 TO 6.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.2 TO 6.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.4 TO 6.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.6 TO 6.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.8 TO 7.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.0 TO 7.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.2 TO 7.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.4 TO 7.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.6 TO 7.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.8 TO 8.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.0 TO 8.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.2 TO 8.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

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 1 *****PLUME LENGTH-K-STABILITY FREQUENCY
 TABLE*****
 Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

| CATEGORY 3 PLUME | | STABILITY CATEGORY 1 | | | STABILITY CATEGORY 2 | | | STABILITY |
|---------------------|--------|----------------------|-------|-------|----------------------|-------|-------|-----------|
| LENGTH RANGE (M) | | K1 | K2 | K3 | K1 | K2 | K3 | K1 |
| K2 | K3 | -- | -- | -- | -- | -- | -- | -- |
| -- | -- | | | | | | | |
| 0.0 | TO 0.2 | 0.000 | 0.000 | 0.152 | 0.000 | 0.000 | 0.568 | 0.000 |
| 0.000 | 0.112 | | | | | | | |
| 0.2 | TO 0.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 0.4 | TO 0.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 0.6 | TO 0.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 0.8 | TO 1.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 1.0 | TO 1.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 1.2 | TO 1.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 1.4 | TO 1.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 1.6 | TO 1.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 1.8 | TO 2.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 2.0 | TO 2.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 2.2 | TO 2.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 2.4 | TO 2.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 2.6 | TO 2.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 2.8 | TO 3.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 3.0 | TO 3.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 3.2 | TO 3.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 3.4 | TO 3.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 3.6 | TO 3.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 3.8 | TO 4.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 4.0 | TO 4.2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 4.2 | TO 4.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 4.4 | TO 4.6 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 4.6 | TO 4.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 4.8 | TO 5.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |

| Length Range (m) | K1 | K2 | K3 | prep | K1 | K2 | K3 | Stability |
|------------------|-------|-------|-------|------|-------|-------|-------|-----------|
| 5.0 TO 5.2 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 5.2 TO 5.4 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 5.4 TO 5.6 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 5.6 TO 5.8 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 5.8 TO 6.0 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 6.0 TO 6.2 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 6.2 TO 6.4 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 6.4 TO 6.6 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 6.6 TO 6.8 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 6.8 TO 7.0 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 7.0 TO 7.2 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 7.2 TO 7.4 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 7.4 TO 7.6 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 7.6 TO 7.8 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 7.8 TO 8.0 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 8.0 TO 8.2 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 8.2 TO 8.4 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 8.4 TO 8.6 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 8.6 TO 8.8 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 8.8 TO 9.0 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 9.0 TO 9.2 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 9.2 TO 9.4 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 9.4 TO 9.6 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 9.6 TO 9.8 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |
| 9.8 TO 10.0 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | |

1 *****PLUME LENGTH-K-STABILITY FREQUENCY
 TABLE*****
 Northern Michigan University - MARQUETTE - COOLING TOWER ANALYSIS (NTH)

| CATEGORY 3 PLUME LENGTH RANGE (M) | STABILITY CATEGORY 1 | | | STABILITY CATEGORY 2 | | | STABILITY |
|---|----------------------|-------|-------|----------------------|-------|-------|-----------|
| | K1 | K2 | K3 | K1 | K2 | K3 | K1 |
| 10.0 TO 10.4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

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| | | | | | | | | |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.000 | 0.000 | | | | | | | |
| 10.4 TO 10.8 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 10.8 TO 11.2 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 11.2 TO 11.6 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 11.6 TO 12.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 12.0 TO 12.4 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 12.4 TO 12.8 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 12.8 TO 13.2 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 13.2 TO 13.6 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 13.6 TO 14.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 14.0 TO 14.4 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 14.4 TO 14.8 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 14.8 TO 15.2 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 15.2 TO 15.6 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 15.6 TO 16.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 16.0 TO 16.4 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 16.4 TO 16.8 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 16.8 TO 17.2 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 17.2 TO 17.6 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 17.6 TO 18.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.003 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 18.0 TO 18.4 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 18.4 TO 18.8 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 | 0.001 | | | | | | | |
| 18.8 TO 19.2 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 19.2 TO 19.6 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 19.6 TO 20.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.000 |
| 0.000 | 0.001 | | | | | | | |
| 20.0 TO 21.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.003 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 21.0 TO 22.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.000 |
| 0.000 | 0.003 | | | | | | | |
| 22.0 TO 23.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.003 | 0.000 |
| 0.000 | 0.001 | | | | | | | |
| 23.0 TO 24.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.002 | 0.000 |
| 0.000 | 0.002 | | | | | | | |
| 24.0 TO 25.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.005 | 0.000 |
| 0.000 | 0.001 | | | | | | | |
| 25.0 TO 26.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.004 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 26.0 TO 27.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.003 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 27.0 TO 28.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.004 | 0.000 |
| 0.000 | 0.000 | | | | | | | |
| 28.0 TO 29.0 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.003 | 0.000 |
| 0.000 | 0.000 | | | | | | | |

| | | prep | | | | | | | |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 29.0 TO 30.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.004 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |
| 30.0 TO 31.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |
| 31.0 TO 32.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |
| 32.0 TO 33.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |
| 33.0 TO 34.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |
| 34.0 TO 35.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |
| 35.0 TO 36.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |
| 36.0 TO 37.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |
| 37.0 TO 38.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |
| 38.0 TO 39.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |
| 39.0 TO 40.0 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |
| 40.0 TO OVER | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.000 0.000 | | | | | | | | | |

1 CAT NUM TYPE UH WX DBT DTDZ DPT VE TE MXHT PLGT
 FREQ REFERENCE HEIGHT= 10. M

| | | | | | | | | | | | |
|--------|----|-------|------|------|-------|--------|-------|-----|-------|-------|-------|
| 0.0012 | 1 | FOG | 10.0 | 0.25 | 263.1 | -0.010 | 262.6 | 0.3 | 270.1 | 500. | 6.24 |
| 0.0004 | 2 | FOG | 15.0 | 0.25 | 263.1 | -0.010 | 262.6 | 0.3 | 270.1 | 500. | 0.00 |
| 0.0037 | 3 | FOG | 12.0 | 0.25 | 263.1 | -0.010 | 261.1 | 0.3 | 269.8 | 500. | 0.00 |
| 0.0004 | 4 | FOG | 17.0 | 0.25 | 263.1 | -0.010 | 261.1 | 0.3 | 269.8 | 500. | 0.00 |
| 0.0003 | 5 | FOG | 15.0 | 0.25 | 263.1 | -0.010 | 258.6 | 0.3 | 269.4 | 500. | 0.00 |
| 0.0036 | 6 | FOG | 12.5 | 0.25 | 273.1 | -0.010 | 272.4 | 0.3 | 278.5 | 500. | 0.00 |
| 0.0009 | 7 | FOG | 16.5 | 0.25 | 273.1 | -0.010 | 269.4 | 0.3 | 277.6 | 500. | 0.00 |
| 0.0007 | 8 | FOG | 15.0 | 0.25 | 283.1 | -0.010 | 282.4 | 0.3 | 286.9 | 500. | 0.00 |
| 0.0001 | 9 | FOG | 16.5 | 0.25 | 283.1 | -0.010 | 279.4 | 0.3 | 285.6 | 500. | 0.00 |
| 0.0001 | 10 | FOG | 15.5 | 0.25 | 293.1 | -0.010 | 291.1 | 0.3 | 294.9 | 500. | 0.00 |
| 0.1517 | 11 | PLUME | 3.9 | 0.15 | 289.6 | -0.018 | 279.4 | 0.3 | 288.1 | 868. | 0.00 |
| 0.6676 | 12 | PLUME | 4.9 | 0.25 | 278.5 | -0.010 | 273.9 | 0.3 | 281.5 | 850. | 9.48 |
| 0.1118 | 13 | PLUME | 2.2 | 0.30 | 277.0 | 0.030 | 273.7 | 0.3 | 280.8 | 950. | 18.88 |
| 0.0001 | 14 | PLUME | 8.7 | 0.25 | 271.0 | -0.010 | 270.9 | 0.3 | 276.9 | 632. | 0.00 |
| 0.0001 | 15 | PLUME | 7.7 | 0.25 | 275.4 | -0.010 | 275.3 | 0.3 | 280.6 | 1120. | 1.17 |
| 0.0003 | 16 | PLUME | 4.6 | 0.25 | 292.1 | -0.010 | 292.0 | 0.3 | 295.1 | 996. | 1.73 |
| 0.0003 | 17 | PLUME | 5.7 | 0.25 | 285.4 | -0.010 | 285.3 | 0.3 | 289.2 | 730. | 2.58 |
| 0.0005 | 18 | PLUME | 7.7 | 0.25 | 274.3 | -0.010 | 274.2 | 0.3 | 279.7 | 984. | 3.38 |
| | 19 | PLUME | 5.7 | 0.25 | 285.1 | -0.010 | 285.0 | 0.3 | 288.9 | 620. | 3.20 |

| | | | | | prep | | | | | | |
|--------|----|-------|-----|------|-------|--------|-------|-----|-------|-------|-------|
| 0.0004 | 20 | PLUME | 4.6 | 0.25 | 290.4 | -0.010 | 290.3 | 0.3 | 293.6 | 426. | 4.17 |
| 0.0001 | 21 | PLUME | 5.8 | 0.25 | 283.4 | -0.010 | 283.3 | 0.3 | 287.4 | 671. | 4.44 |
| 0.0004 | 22 | PLUME | 7.2 | 0.25 | 276.0 | -0.010 | 275.9 | 0.3 | 281.1 | 689. | 5.10 |
| 0.0001 | 23 | PLUME | 4.6 | 0.25 | 285.4 | -0.010 | 285.3 | 0.3 | 289.2 | 800. | 11.31 |
| 0.0001 | 24 | PLUME | 6.2 | 0.25 | 281.0 | -0.010 | 280.9 | 0.3 | 285.4 | 782. | 5.47 |
| 0.0005 | 25 | PLUME | 3.6 | 0.25 | 292.1 | -0.010 | 292.0 | 0.3 | 295.1 | 923. | 10.12 |
| 0.0001 | 26 | PLUME | 4.9 | 0.25 | 287.6 | -0.010 | 287.5 | 0.3 | 291.1 | 836. | 6.03 |
| 0.0003 | 27 | PLUME | 5.1 | 0.25 | 285.4 | -0.010 | 285.3 | 0.3 | 289.2 | 904. | 7.21 |
| 0.0003 | 28 | PLUME | 7.7 | 0.25 | 272.1 | -0.010 | 272.0 | 0.3 | 277.8 | 766. | 7.69 |
| 0.0001 | 29 | PLUME | 4.1 | 0.25 | 291.0 | -0.010 | 290.9 | 0.3 | 294.1 | 496. | 7.72 |
| 0.0001 | 30 | PLUME | 5.7 | 0.25 | 282.1 | -0.010 | 282.0 | 0.3 | 286.3 | 1046. | 8.15 |
| 0.0004 | 31 | PLUME | 6.2 | 0.25 | 279.3 | -0.010 | 279.2 | 0.3 | 283.9 | 771. | 8.39 |
| 0.0001 | 32 | PLUME | 4.9 | 0.25 | 285.7 | -0.010 | 285.6 | 0.3 | 289.4 | 784. | 8.93 |
| 0.0003 | 33 | PLUME | 4.1 | 0.25 | 286.0 | -0.010 | 285.9 | 0.3 | 289.7 | 11. | 14.07 |
| 0.0001 | 34 | PLUME | 5.7 | 0.25 | 281.0 | -0.010 | 280.9 | 0.3 | 285.4 | 1028. | 9.97 |
| 0.0001 | 35 | PLUME | 5.4 | 0.25 | 281.2 | -0.010 | 281.1 | 0.3 | 285.5 | 726. | 12.08 |
| 0.0007 | 36 | PLUME | 5.7 | 0.25 | 280.8 | -0.010 | 280.7 | 0.3 | 285.2 | 631. | 10.33 |
| 0.0007 | 37 | PLUME | 4.2 | 0.25 | 287.6 | -0.010 | 287.5 | 0.3 | 291.1 | 830. | 11.12 |
| 0.0005 | 38 | PLUME | 3.6 | 0.25 | 289.6 | -0.010 | 289.5 | 0.3 | 292.8 | 902. | 12.95 |
| 0.0003 | 39 | PLUME | 4.6 | 0.25 | 284.3 | -0.010 | 284.2 | 0.3 | 288.2 | 767. | 12.85 |
| 0.0004 | 40 | PLUME | 5.1 | 0.25 | 282.1 | -0.010 | 282.0 | 0.3 | 286.3 | 676. | 12.29 |
| 0.0005 | 41 | PLUME | 5.9 | 0.25 | 278.1 | -0.010 | 278.0 | 0.3 | 282.9 | 610. | 12.64 |
| 0.0005 | 42 | PLUME | 3.1 | 0.25 | 292.1 | -0.010 | 292.0 | 0.3 | 295.1 | 603. | 13.13 |
| 0.0003 | 43 | PLUME | 3.6 | 0.25 | 283.9 | -0.010 | 283.8 | 0.3 | 287.9 | 701. | 18.87 |
| 0.0127 | 44 | PLUME | 2.9 | 0.25 | 277.5 | -0.010 | 277.4 | 0.3 | 282.4 | 604. | 24.83 |
| 0.0298 | 45 | PLUME | 3.3 | 0.25 | 271.6 | -0.010 | 271.6 | 0.3 | 277.4 | 605. | 29.10 |
| 0.0174 | | | | | | | | | | | |

MET RECORDS READ : 8760
RECORDS DISCARDED: 0
CALM RECORDS: 1284

TOTAL TO NEW FILE: 8760



APPENDIX G

Visibility Modeling Support Information

| | | | | | | | |
|---|-----------------|-----------------|---------------|---------------|---------------|---------------|---------------|
| Major Pollutants | SO ₂ | NO _x | CO | PM | VOCs | HAPs | Radionuclides |
| Maximum Hourly Allowable (MHA) (lb/day) | 10.7 | 11.5 | 11.5 | 11.5 | 11.5 | 11.5 | 11.5 |
| Annual Allowable (AL) (lb/year) | 3880 | 4020 | 4020 | 4020 | 4020 | 4020 | 4020 |
| CFR Section | 40 CFR 61.105 | 40 CFR 61.105 | 40 CFR 61.105 | 40 CFR 61.105 | 40 CFR 61.105 | 40 CFR 61.105 | 40 CFR 61.105 |

(Applicable to Category 7)

| Material | Mercury Content (%) | Mercury (lb/year) | Mercury (lb/day) | Mercury (lb/hr) | Mercury (lb/min) | Mercury (lb/1000 lbs) |
|----------|---------------------|-------------------|------------------|-----------------|------------------|-----------------------|
| 304 SS | 0.0012 | 1.2 | 0.0034 | 0.00008 | 0.000001 | 0.1014 |
| 316 SS | 0.0012 | 1.2 | 0.0034 | 0.00008 | 0.000001 | 0.1014 |
| 309 SS | 0.0012 | 1.2 | 0.0034 | 0.00008 | 0.000001 | 0.1014 |
| 310 SS | 0.0012 | 1.2 | 0.0034 | 0.00008 | 0.000001 | 0.1014 |

TABLE B-1. EMISSION RATES OF CRITERIA POLLUTANTS, HAPs, AND TACs FROM THE NEW BOILER ON A PER-FUEL BASIS

| Compounds | CAS Reference Number | Coal | | Fuel Oil | | Natural Gas | | Waste Oil | | Waste Sludge | | Fuel |
|---|----------------------|-------|--------|----------|--------|-------------|--------|-----------|--------|--------------|--------|------|
| | | lb/hr | lb/day | lb/hr | lb/day | lb/hr | lb/day | lb/hr | lb/day | lb/hr | lb/day | |
| Carbon monoxide | 63002 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| Carbon dioxide | 74402 | 11.5 | 276 | 11.5 | 276 | 11.5 | 276 | 11.5 | 276 | 11.5 | 276 | Wood |
| Carbon disulfide | 75632 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| Carbon tetrachloride | 56188 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| Chlorobenzene | 70832 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| Chloroform | 67627 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| Chlorophenol | 10647 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,1-Dichloroethane | 78041 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2-Dichloroethane | 10706 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,1,1-Trichloroethane | 70832 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,1,2-Trichloroethane | 78041 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,2-Trichloroethane | 78041 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,1,1,1-Tetrachloroethane | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,1,1,2-Tetrachloroethane | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,1,2,2-Tetrachloroethane | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,1,2,2,2-Pentachloroethane | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,1,1,1,2-Pentachloroethane | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,1,1,1,2,2-Hexachloroethane | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,1,1,2,2,2-Hexachloroethane | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,1,2,2,3,3-Hexachloroethane | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,2,3,3,3-Hexachloroethane | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (alpha) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (beta) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (gamma) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (delta) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (epsilon) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (zeta) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (eta) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (theta) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (iota) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (kappa) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (lambda) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (mu) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (nu) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (xi) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (omicron) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (pi) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (rho) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (sigma) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (tau) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (upsilon) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (phi) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (chi) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (psi) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |
| 1,2,3,4,5,6-Hexachlorocyclohexane (omega) | 79069 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | 0.001 | 0.024 | Wood |

Proposed Circulating Fluidized Bed Boiler
Potential Emissions

Northern Michigan University
Marquette, MI
CFS Boiler Project

| Compound | Refill Content | Material Usage (lb) | Weight (lb) | Usage (BTU/hr) | Heating Value (BTU/lb) | Market Throughput (lb/yr) | Market Throughput (lb/yr) | Market Throughput (lb/yr) | Market Throughput (lb/yr) | Market Throughput (lb/yr) | Market Throughput (lb/yr) | Market Throughput (lb/yr) | Market Throughput (lb/yr) |
|----------|----------------|---------------------|-------------|----------------|------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| Coal | 3.00% | 3,000 | 3,000 | 3,000 | 3,000 | 3,000 | 3,000 | 3,000 | 3,000 | 3,000 | 3,000 | 3,000 | 3,000 |
| Oil | 0.00% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Gas | 0.00% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Wood | 0.00% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other | 0.00% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

(Approximate values only)

| Compound | Coal Emissions | | | | Oil Emissions | | | | Gas Emissions | | | | Wood Emissions | | | | Emission Rate (lb/yr) | Emission Rate (lb/yr) | Emission Rate (lb/yr) | Emission Rate (lb/yr) | | | | | | |
|------------------|----------------|------|-------|------|---------------|------|-------|------|---------------|------|-------|------|----------------|------|-------|------|-----------------------|-----------------------|-----------------------|-----------------------|-------|------|------|----|------|----|
| | Value | Unit | Value | Unit | Value | Unit | Value | Unit | Value | Unit | Value | Unit | Value | Unit | Value | Unit | | | | | Value | Unit | | | | |
| SO ₂ | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | | | | | | |
| NO _x | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | | | | |
| CO | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | | |
| PM ₁₀ | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb |

TABLE B-1. EMISSION RATES OF CRITERIA POLLUTANTS, HAPs, AND TAGS FROM THE NEW BOILER ON A PER-FUEL BASIS

| Compound | CAS Reference Number | Coal Emissions | | | | Oil Emissions | | | | Gas Emissions | | | | Wood Emissions | | | | Emission Rate (lb/yr) | Emission Rate (lb/yr) | Emission Rate (lb/yr) | Emission Rate (lb/yr) | | | | | | | | | | | | | | | | | | | | |
|------------------|----------------------|----------------|------|-------|------|---------------|------|-------|------|---------------|------|-------|------|----------------|------|-------|------|-----------------------|-----------------------|-----------------------|-----------------------|-------|------|------|----|------|----|------|----|------|----|------|----|------|----|------|----|------|----|------|----|
| | | Value | Unit | Value | Unit | Value | Unit | Value | Unit | Value | Unit | Value | Unit | Value | Unit | Value | Unit | | | | | Value | Unit | | | | | | | | | | | | | | | | | | |
| SO ₂ | 7446-08-6 | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb |
| NO _x | 10102-43-9 | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb |
| CO | 68-01-9 | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb |
| PM ₁₀ | 14303-37-3 | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb | 0.00 | lb |

NMU Updraft Emission Streamhead for SO₂ on Oil Coal - Fulls 100%

TABLE B-2. MAXIMUM EMISSION RATES

| Compound | Maximum Emission Rates | | | |
|------------------|------------------------|-------|-------|-------|
| | Value | Unit | Value | Unit |
| SO ₂ | 0.00 | lb/yr | 0.00 | lb/yr |
| NO _x | 0.00 | lb/yr | 0.00 | lb/yr |
| CO | 0.00 | lb/yr | 0.00 | lb/yr |
| PM ₁₀ | 0.00 | lb/yr | 0.00 | lb/yr |

| Boiler Parameters | Specification |
|--------------------------------|---------------------------|
| Boiler Type | Circulating Fluidized Bed |
| Medium Pressure Heat Exchanger | 15 15 |
| Operating Pressure | 15 |
| Design Life (Years) | 15 |

(Approximate, normally 7)

| Material | Bulk Content | Heat Input BTU/hr | Heating Value (BTU/lb) | Material Throughput (lb/hr) | Material Throughput (tph) | Natural Gas Maximum Usage Rate (tph) |
|----------|--------------|-------------------|------------------------|-----------------------------|---------------------------|--------------------------------------|
| Coal | 100.0% | 15 | 12,500 | 300 | 66,933 | |
| Oil | 0.0% | 10 | 17,800 | 100 | 66,933 | |
| Gas | 100.0% | 10 | 17,800 | 100 | 66,933 | 0.1014 |

TABLE B-1. EMISSION RATES OF CRITERIA POLLUTANTS, HAPS, AND TAGS FROM THE NEW BOILER ON A PER-FUEL BASIS

| Compound | CAS Reference Number | Coal Biomass | | Coal FFB | | Natural Gas | | Waste Wood | | Emission Rates | | Emission Factor | Fuel | Emission Rate |
|---------------------------|----------------------|--------------|-------|----------|-------|-------------|-------|------------|-------|----------------|-------|-----------------|------|---------------|
| | | Value | Units | Value | Units | Value | Units | Value | Units | Value | Units | | | |
| | | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | | | | | | | |
| 1,1,1-Trichloroethane | 70824 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,1,2-Dichloroethane | 78168 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,1,2,2-Tetrachloroethane | 60092 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dichloroethane | 108054 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 79014 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dichlorobenzene | 133207 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 6476 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 8329 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 20598 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 6784 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 10027 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 5689 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 5038 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 19272 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 20592 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 20540 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 20523 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 9042 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 9044 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11707 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11709 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11710 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11711 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11712 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11713 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11714 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11715 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11716 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11717 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11718 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11719 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11720 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11721 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11722 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11723 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11724 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |
| 1,2-Dibromobenzene | 11725 | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 0.002 | lb/hr | 1.50E-03 | Wood | 1.00E-03 |

CFB Boiler Maximum Single HAP Emission Rate (HCl) = 6.3 tpy
CFB Boiler Maximum Combined Total HAP Emission Rate = 22.7 tpy

These emission rates are based on the EPA AP-42 database, and are increased by a 10% safety factor unless otherwise noted below. Emission factors are based on the EPA AP-42 database. Coal firing emission factor based on dry FFB. Emission factors are based on the EPA AP-42 database. Both HCl and HBr emission factors include a 15% safety factor and 92% control using lime in the CFB. Emissions are based on the proposed EACT. Sulfate acid mist emission based on HCLC search. Plant Nth Energy entry. This facility is located in Adhesia. Total dust/PM for the coal firing is from the Wyodah energy stack test results, and contribution for the wood combustion is from the EPA AP-42, Chapter 1.6, Table 1.5-3. Total chromium is supplied here for information purposes only. Total Chromium is a sum of hexavalent and trivalent chromium.

NMCA Updated Emission Spreadsheet for % on Bit Coal Furnace 100%



APPENDIX B
Emission Summary Tables

| Boiler Parameter | Specification | |
|--------------------------------------|---------------|-----------------------|
| | Boiler Vendor | Original Manufacturer |
| Maximum Rated Heat Input (MM Btu/hr) | 16 | 16 |
| Net Capacity (MM Btu/hr) | 16 | 16 |
| Steam Output (MMBtu/hr) | 16 | 16 |

| Material | Sulfur Content | Moisture (%) | Heat Input (MM BTU/hr) | Heating Value (BTU/lb) | Material Throughput (tpd) | Material Throughput (tpd) | Natural Gas Usage Rate (Mcf/hr) |
|----------|----------------|--------------|------------------------|------------------------|---------------------------|---------------------------|---------------------------------|
| Coal | 0.008 | 17.50 | 55 | 15,000 | 35 | 28 | 0.1814 |
| Coal | 0.008 | 17.50 | 55 | 15,000 | 35 | 28 | |
| Coal | 0.008 | 17.50 | 55 | 15,000 | 35 | 28 | |
| Coal | 0.008 | 17.50 | 55 | 15,000 | 35 | 28 | |
| Coal | 0.008 | 17.50 | 55 | 15,000 | 35 | 28 | |
| Coal | 0.008 | 17.50 | 55 | 15,000 | 35 | 28 | |

TABLE B-1. EMISSION RATES OF CRITERIA POLLUTANTS, HAPS, AND TAGS FROM THE NEW BOILER ON A PER-FUEL BASIS

| Compound | Coal, Bituminous | | | | | | | | Coke, PRB | | | | | Natural Gas | | | | | Waste Wood | | | | | | | |
|--|-----------------------|------------------|----------|-------|----------------|-------|----------|----------------|-----------|-------|----------------|-------|----------|----------------|----------|-------|----------------|-------|------------|----------------|----------|-------|----------|-------|----------|-------|
| | CA's Reference Number | Emission Factors | Value | Units | Emission Rates | Value | Units | Emission Rates | Value | Units | Emission Rates | Value | Units | Emission Rates | Value | Units | Emission Rates | Value | Units | Emission Rates | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | (lb/tpd) | (tpd) | (lb/tpd) | (tpd) | (lb/tpd) | (tpd) |
| PAHs (Meribla and condensable) | | | 0.32 | tpd | 0.32 | tpd | 0.32 | tpd | 0.32 | tpd | 0.32 | tpd | 0.32 | tpd | 0.32 | tpd | 0.32 | tpd | 0.32 | tpd | 0.32 | tpd | 0.32 | tpd | | |
| SO ₂ | | | 0.475 | tpd | 0.475 | tpd | 0.475 | tpd | 0.475 | tpd | 0.475 | tpd | 0.475 | tpd | 0.475 | tpd | 0.475 | tpd | 0.475 | tpd | 0.475 | tpd | 0.475 | tpd | 0.475 | tpd |
| NO _x | | | 0.10 | tpd | 0.10 | tpd | 0.10 | tpd | 0.10 | tpd | 0.10 | tpd | 0.10 | tpd | 0.10 | tpd | 0.10 | tpd | 0.10 | tpd | 0.10 | tpd | 0.10 | tpd | 0.10 | tpd |
| CO | | | 1.34E-05 | tpd | 1.34E-05 | tpd | 1.34E-05 | tpd | 1.34E-05 | tpd | 1.34E-05 | tpd | 1.34E-05 | tpd | 1.34E-05 | tpd | 1.34E-05 | tpd | 1.34E-05 | tpd | 1.34E-05 | tpd | 1.34E-05 | tpd | 1.34E-05 | tpd |
| NO ₂ (As Sulfate Acid Mass) | | | 3.00E-09 | tpd | 3.00E-09 | tpd | 3.00E-09 | tpd | 3.00E-09 | tpd | 3.00E-09 | tpd | 3.00E-09 | tpd | 3.00E-09 | tpd | 3.00E-09 | tpd | 3.00E-09 | tpd | 3.00E-09 | tpd | 3.00E-09 | tpd | 3.00E-09 | tpd |
| VOC | | | 0.02 | tpd | 0.02 | tpd | 0.02 | tpd | 0.02 | tpd | 0.02 | tpd | 0.02 | tpd | 0.02 | tpd | 0.02 | tpd | 0.02 | tpd | 0.02 | tpd | 0.02 | tpd | 0.02 | tpd |
| Mercury | | | 0.11 | tpd | 0.11 | tpd | 0.11 | tpd | 0.11 | tpd | 0.11 | tpd | 0.11 | tpd | 0.11 | tpd | 0.11 | tpd | 0.11 | tpd | 0.11 | tpd | 0.11 | tpd | 0.11 | tpd |
| HF | | | 0.01 | tpd | 0.01 | tpd | 0.01 | tpd | 0.01 | tpd | 0.01 | tpd | 0.01 | tpd | 0.01 | tpd | 0.01 | tpd | 0.01 | tpd | 0.01 | tpd | 0.01 | tpd | 0.01 | tpd |
| Total Dioxin/Furan* | | | 0.11E-03 | tpd | 0.11E-03 | tpd | 0.11E-03 | tpd | 0.11E-03 | tpd | 0.11E-03 | tpd | 0.11E-03 | tpd | 0.11E-03 | tpd | 0.11E-03 | tpd | 0.11E-03 | tpd | 0.11E-03 | tpd | 0.11E-03 | tpd | 0.11E-03 | tpd |
| Metals | | | 2.34E-10 | tpd | 2.34E-10 | tpd | 2.34E-10 | tpd | 2.34E-10 | tpd | 2.34E-10 | tpd | 2.34E-10 | tpd | 2.34E-10 | tpd | 2.34E-10 | tpd | 2.34E-10 | tpd | 2.34E-10 | tpd | 2.34E-10 | tpd | 2.34E-10 | tpd |
| Antimony | | | 0.05E-06 | tpd | 0.05E-06 | tpd | 0.05E-06 | tpd | 0.05E-06 | tpd | 0.05E-06 | tpd | 0.05E-06 | tpd | 0.05E-06 | tpd | 0.05E-06 | tpd | 0.05E-06 | tpd | 0.05E-06 | tpd | 0.05E-06 | tpd | 0.05E-06 | tpd |
| Arsenic | | | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd |
| Boron | | | 2.00E-06 | tpd | 2.00E-06 | tpd | 2.00E-06 | tpd | 2.00E-06 | tpd | 2.00E-06 | tpd | 2.00E-06 | tpd | 2.00E-06 | tpd | 2.00E-06 | tpd | 2.00E-06 | tpd | 2.00E-06 | tpd | 2.00E-06 | tpd | 2.00E-06 | tpd |
| Barium | | | 0.00E-08 | tpd | 0.00E-08 | tpd | 0.00E-08 | tpd | 0.00E-08 | tpd | 0.00E-08 | tpd | 0.00E-08 | tpd | 0.00E-08 | tpd | 0.00E-08 | tpd | 0.00E-08 | tpd | 0.00E-08 | tpd | 0.00E-08 | tpd | 0.00E-08 | tpd |
| Beryllium | | | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd |
| Cadmium | | | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd | 1.20E-06 | tpd |
| Chromium, total | | | 3.95E-07 | tpd | 3.95E-07 | tpd | 3.95E-07 | tpd | 3.95E-07 | tpd | 3.95E-07 | tpd | 3.95E-07 | tpd | 3.95E-07 | tpd | 3.95E-07 | tpd | 3.95E-07 | tpd | 3.95E-07 | tpd | 3.95E-07 | tpd | 3.95E-07 | tpd |
| Chromium, hexavalent* | | | 8.37E-07 | tpd | 8.37E-07 | tpd | 8.37E-07 | tpd | 8.37E-07 | tpd | 8.37E-07 | tpd | 8.37E-07 | tpd | 8.37E-07 | tpd | 8.37E-07 | tpd | 8.37E-07 | tpd | 8.37E-07 | tpd | 8.37E-07 | tpd | 8.37E-07 | tpd |
| Chromium, trivalent* | | | 1.15E-04 | tpd | 1.15E-04 | tpd | 1.15E-04 | tpd | 1.15E-04 | tpd | 1.15E-04 | tpd | 1.15E-04 | tpd | 1.15E-04 | tpd | 1.15E-04 | tpd | 1.15E-04 | tpd | 1.15E-04 | tpd | 1.15E-04 | tpd | 1.15E-04 | tpd |
| Cobalt | | | 1.27E-02 | tpd | 1.27E-02 | tpd | 1.27E-02 | tpd | 1.27E-02 | tpd | 1.27E-02 | tpd | 1.27E-02 | tpd | 1.27E-02 | tpd | 1.27E-02 | tpd | 1.27E-02 | tpd | 1.27E-02 | tpd | 1.27E-02 | tpd | 1.27E-02 | tpd |
| Copper | | | 7.89E-08 | tpd | 7.89E-08 | tpd | 7.89E-08 | tpd | 7.89E-08 | tpd | 7.89E-08 | tpd | 7.89E-08 | tpd | 7.89E-08 | tpd | 7.89E-08 | tpd | 7.89E-08 | tpd | 7.89E-08 | tpd | 7.89E-08 | tpd | 7.89E-08 | tpd |
| Iron | | | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd |
| Magnesium | | | 9.30E-06 | tpd | 9.30E-06 | tpd | 9.30E-06 | tpd | 9.30E-06 | tpd | 9.30E-06 | tpd | 9.30E-06 | tpd | 9.30E-06 | tpd | 9.30E-06 | tpd | 9.30E-06 | tpd | 9.30E-06 | tpd | 9.30E-06 | tpd | 9.30E-06 | tpd |
| Manganese | | | 1.72E-03 | tpd | 1.72E-03 | tpd | 1.72E-03 | tpd | 1.72E-03 | tpd | 1.72E-03 | tpd | 1.72E-03 | tpd | 1.72E-03 | tpd | 1.72E-03 | tpd | 1.72E-03 | tpd | 1.72E-03 | tpd | 1.72E-03 | tpd | 1.72E-03 | tpd |
| Molybdenum | | | 1.87E-06 | tpd | 1.87E-06 | tpd | 1.87E-06 | tpd | 1.87E-06 | tpd | 1.87E-06 | tpd | 1.87E-06 | tpd | 1.87E-06 | tpd | 1.87E-06 | tpd | 1.87E-06 | tpd | 1.87E-06 | tpd | 1.87E-06 | tpd | 1.87E-06 | tpd |
| Nickel | | | 3.00E-04 | tpd | 3.00E-04 | tpd | 3.00E-04 | tpd | 3.00E-04 | tpd | 3.00E-04 | tpd | 3.00E-04 | tpd | 3.00E-04 | tpd | 3.00E-04 | tpd | 3.00E-04 | tpd | 3.00E-04 | tpd | 3.00E-04 | tpd | 3.00E-04 | tpd |
| Phosphorus | | | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd |
| Potassium | | | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd | 1.00E-02 | tpd |
| Selenium | | | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd |
| Silver | | | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd |
| Sodium | | | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd |
| Strontium | | | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd |
| Tin | | | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd |
| Titanium | | | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd |
| Vanadium | | | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd |
| Zinc | | | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd | 0.00E-06 | tpd |
| Organic Compounds | | | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd |
| Acetaldehyde | | | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd |
| Acrylonitrile | | | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd |
| Acrylonitrile | | | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd | | tpd |
| Benzene | | | | tpd | | tpd | | tpd | | tpd | | | | | | | | | | | | | | | | |



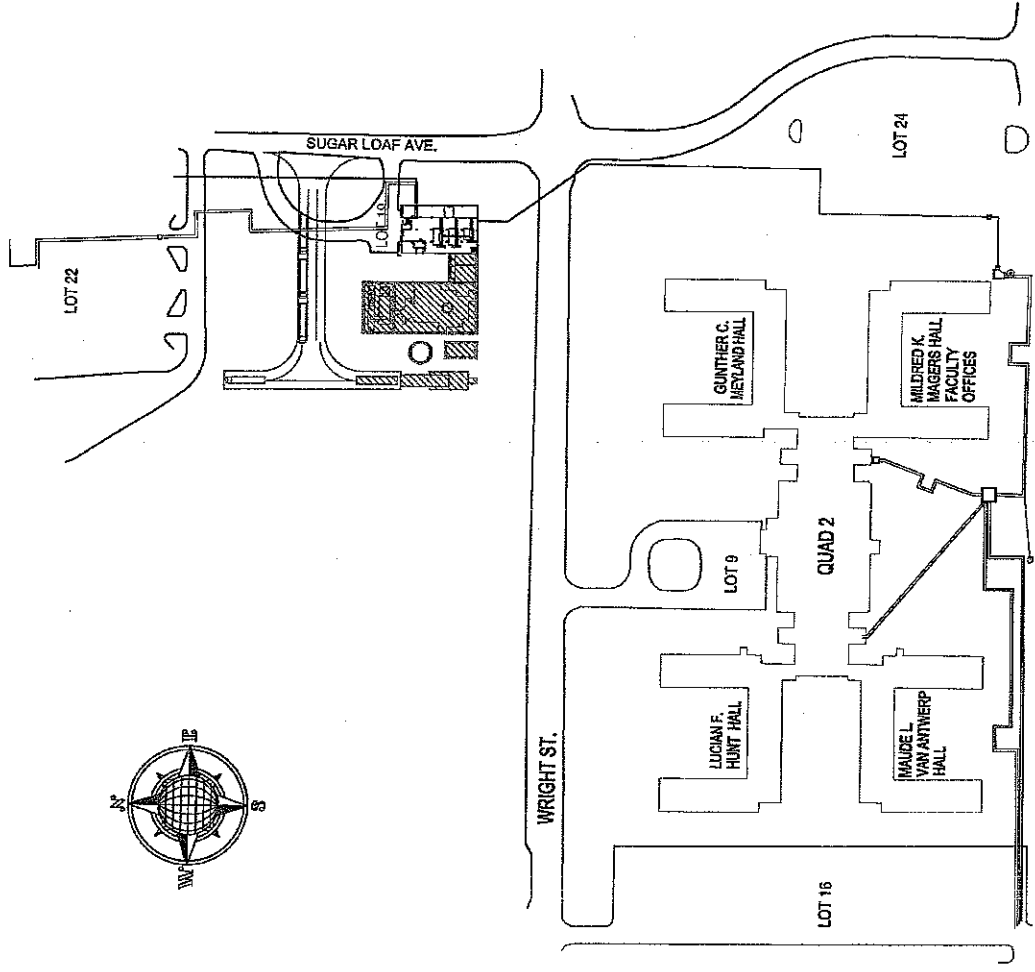
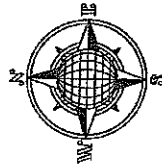
APPENDIX A
Site Drawings



CAMPUS MAP - NORTHERN SECTION

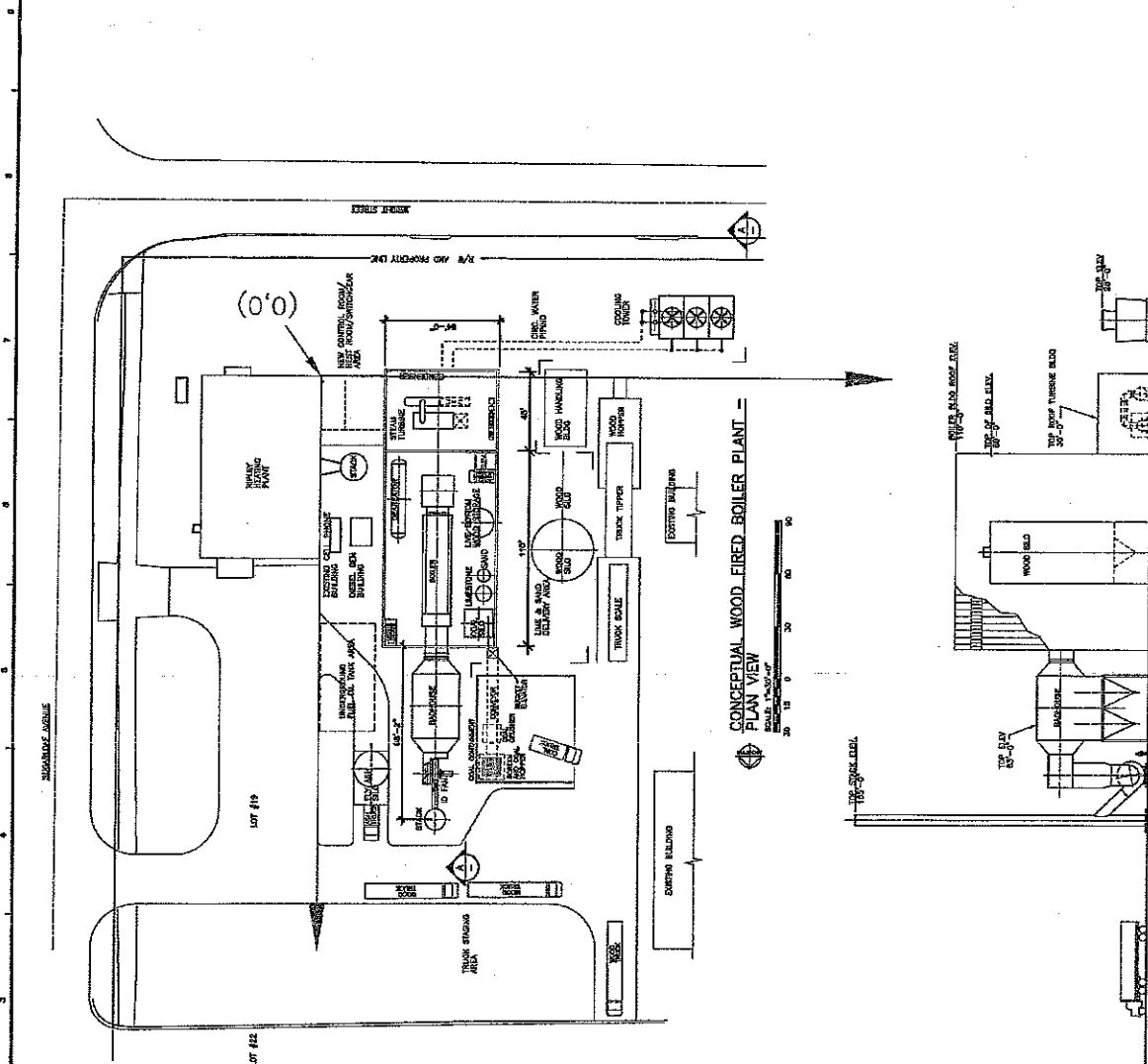
NORTHERN MICHIGAN UNIVERSITY

MARQUETTE, MICHIGAN
DATE: SEPTEMBER 4, 2003



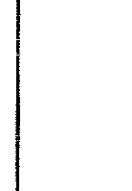
| ELECTRICAL LEGEND | |
|-------------------|-------------------------|
| SYMBOL | UTILITY |
| ⊛ | ELECTRIC |
| ⊛ | HIGH WATT LIGHTPOLE |
| ⊛ | SINGLE SHROUD LIGHTPOLE |
| ⊛ | DOUBLE SHROUD LIGHTPOLE |
| ⊛ | QUAD SHROUD LIGHTPOLE |
| ⊛ | LIGHTPOLE |
| ⊛ | CODE BUREAU STATION |
| ⊛ | MANHOLE |
| ⊛ | LIGHTED BUILDING BEAMS |

| STEAM LEGEND | |
|--------------|------------------|
| SYMBOL | UTILITY |
| ⊛ | STEAM |
| ⊛ | ABANDONED STEAM |
| ⊛ | MANHOLE |
| ⊛ | STEAM VAULT (SV) |



SECTION A-A

SECTION A-A



NOT TO BE USED FOR
CONSTRUCTION

| | | | | |
|-----|------|-------------|----|-------|
| NO. | DATE | DESCRIPTION | BY | CHKD. |
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NORTHERN MICHIGAN UNIVERSITY
WOODY/COAL-FIRED BOILER

EQUIPMENT ARRANGEMENT

| | |
|---------------------------|----------------------|
| SCALE: 20" = 1'-0" | PROJECT NO.: 2004.23 |
| DWG. NO.: 5048-CGA-M1001A | REV. A |

| Impact | Averaging Period |
|--------|------------------|
| 0.211 | Annual |
| 1.569 | 24 Hour |
| 2.712 | 8 Hour |
| 15.779 | 1 Hour |

1.0 Gram/Sec Modeled Impacts

**Northern Michigan University
New CFB Boiler
Toxic Air Contaminant Modeling Results**

Table C-1. TAC Emission Rates and Modeling Impact Results

| Compound | CAS No. | Emission Rates | | Modelled Rate (grams/sec) | TRSL (ug/m3) | IRSL (ug/m3) | Averaging Period | Ambient Impact (ug/m ³ / 1 g/s) |
|--------------------------------|------------|----------------|----------|---------------------------|--------------|--------------|------------------|--|
| | | (lb/hr) | (Tpy) | | | | | |
| Lead | 7439-92-1 | 2.49E-03 | 3.12E-04 | 1.5 | 1.5 | 1.5 | 24 hour | 0.03% |
| HCl | 7647-01-0 | 1.20 | 1.61E-01 | 20 | 1.61E-01 | 20 | 24 hour | 1.20% |
| HF | 7664-39-3 | 0.15 | 1.99E-02 | 26 | 1.99E-02 | 26 | 1 hour | 1.15% |
| H ₂ SO ₄ | 7664-39-3 | 1.13 | 1.42E-01 | 494 | 1.42E-01 | 494 | 8 hour | 3.86% |
| Total Dioxin/Furan | 1746-01-6 | 4.33E-10 | 1.80E-09 | 5.45E-11 | 1.80E-09 | 5.45E-11 | Annual | 0.00% |
| Antimony | 7440-36-0 | 1.68E-03 | 7.36E-03 | 2.12E-04 | 7.36E-03 | 2.12E-04 | 24 hour | 0.168% |
| Arsenic | 7440-38-2 | 1.42E-04 | 6.22E-04 | 1.79E-05 | 6.22E-04 | 1.79E-05 | Annual | 1.88% |
| Barium | 7440-39-3 | 9.18E-04 | 4.02E-03 | 1.16E-04 | 4.02E-03 | 1.16E-04 | 8 hour | 0.006% |
| Beryllium | 7440-41-7 | 3.70E-06 | 1.82E-05 | 4.66E-07 | 1.82E-05 | 4.66E-07 | 24 hour | 0.004% |
| Beryllium | 7440-41-7 | 3.70E-06 | 1.82E-05 | 4.66E-07 | 1.82E-05 | 4.66E-07 | 8 hour | 0.004% |
| Cadmium | 7440-43-9 | 2.29E-04 | 1.00E-03 | 2.89E-05 | 1.00E-03 | 2.89E-05 | Annual | 1.02% |
| Chromium, total | 7440-47-3 | 4.95E-03 | 2.17E-02 | 6.24E-04 | 2.17E-02 | 6.24E-04 | Annual | 0.131% |
| Chromium, hexavalent | 18540-29-9 | 8.26E-04 | 3.61E-03 | 1.04E-04 | 3.61E-03 | 1.04E-04 | Annual | 0.17% |
| Chromium, trivalent | 16056-83-1 | 1.55E-04 | 6.78E-04 | 1.96E-05 | 6.78E-04 | 1.96E-05 | Annual | 26.40% |
| Cobalt | 7440-48-4 | 1.25E-03 | 5.49E-03 | 1.58E-04 | 5.49E-03 | 1.58E-04 | 8 hour | 0.001% |
| Copper | 7440-50-9 | 1.16E-04 | 5.08E-04 | 1.46E-05 | 5.08E-04 | 1.46E-05 | 8 hour | 0.214% |
| Copper | 7440-50-9 | 1.16E-04 | 5.08E-04 | 1.46E-05 | 5.08E-04 | 1.46E-05 | 8 hour | 0.002% |
| Iron | 7440-18-0 | 2.33E-03 | 1.02E-02 | 2.94E-04 | 1.02E-02 | 2.94E-04 | Annual | 0.06% |
| Magnesium | 7439-95-4 | 1.38E-01 | 6.03E-01 | 1.73E-02 | 6.03E-01 | 1.73E-02 | 8 hour | 0.047% |
| Manganese | 7439-96-5 | 3.77E-03 | 1.65E-02 | 4.75E-04 | 1.65E-02 | 4.75E-04 | 24 hour | 1.51% |
| Nickel | 7440-02-0 | 3.09E-04 | 1.35E-03 | 3.89E-05 | 1.35E-03 | 3.89E-05 | Annual | 0.20% |
| Nickel | 7440-02-0 | 3.09E-04 | 1.35E-03 | 3.89E-05 | 1.35E-03 | 3.89E-05 | Annual | 0.006% |
| Phosphorus | 7723-14-0 | 6.37E-05 | 2.79E-04 | 8.02E-06 | 2.79E-04 | 8.02E-06 | Annual | 0.002% |
| Potassium | 7782-49-2 | 9.19E-02 | 4.03E-01 | 1.16E-02 | 4.03E-01 | 1.16E-02 | Annual | 2.44% |
| Selenium | 7782-49-2 | 1.63E-02 | 7.16E-02 | 2.06E-03 | 7.16E-02 | 2.06E-03 | 8 hour | 0.279% |
| Selenium | 7782-49-2 | 1.63E-02 | 7.16E-02 | 2.06E-03 | 7.16E-02 | 2.06E-03 | 8 hour | 0.279% |
| Silver | 7440-22-4 | 4.01E-03 | 1.76E-02 | 5.05E-04 | 1.76E-02 | 5.05E-04 | 8 hour | 1.37% |
| Sodium | 8496-04 | 3.72E-03 | 1.07E-04 | 1.07E-04 | 1.07E-04 | 1.07E-04 | Annual | 0.02% |
| Strontium | 206E-05 | 1.03E-04 | 2.97E-06 | 2.97E-06 | 2.97E-06 | 2.97E-06 | Annual | 0.001% |
| Tin | 7440-31-5 | 5.42E-05 | 2.37E-04 | 6.83E-06 | 2.37E-04 | 6.83E-06 | 8 hour | 0.000% |
| Titanium | 4.72E-05 | 2.07E-04 | 5.94E-06 | 5.94E-06 | 2.07E-04 | 5.94E-06 | Annual | 0.001% |
| Vanadium | 4.80E-04 | 2.10E-03 | 6.04E-05 | 6.04E-05 | 2.10E-03 | 6.04E-05 | Annual | 0.013% |
| Zinc (as Zn) | 1314-13-2 | 5.23E-02 | 2.29E-01 | 6.59E-03 | 2.29E-01 | 6.59E-03 | 8 hour | 0.036% |
| Zinc (as Zn) | 1314-13-2 | 5.23E-02 | 2.29E-01 | 6.59E-03 | 2.29E-01 | 6.59E-03 | Annual | 0.000% |
| Acetaldehyde | 75-07-0 | 1.86E-01 | 8.57E-01 | 2.47E-02 | 8.57E-01 | 2.47E-02 | 24 hour | 0.436% |
| Acetophenone | 98-86-2 | 1.88E-04 | 8.22E-04 | 3.07E-05 | 8.22E-04 | 3.07E-05 | 8 hour | 0.000% |
| Acrolein | 107-02-8 | 2.39E-02 | 1.05E-01 | 3.07E-03 | 1.05E-01 | 3.07E-03 | Annual | 3.17% |
| Acrolein | 107-02-8 | 2.39E-02 | 1.05E-01 | 3.07E-03 | 1.05E-01 | 3.07E-03 | 1 hour | 9.50% |
| Benzene | 99-06-0 | 1.05E-01 | 4.34E-00 | 1.25E-01 | 4.34E-00 | 1.25E-01 | 24 hour | 0.66% |
| Benzene | 99-06-0 | 1.05E-01 | 4.34E-00 | 1.25E-01 | 4.34E-00 | 1.25E-01 | Annual | 26.30% |
| Benzyl chloride | 100-44-7 | 8.76E-03 | 3.84E-02 | 1.10E-03 | 3.84E-02 | 1.10E-03 | Annual | 1.16% |
| Benzoinic acid | 65-85-0 | 1.11E-05 | 4.85E-05 | 1.40E-06 | 4.85E-05 | 1.40E-06 | Annual | 0.000% |
| Biphenyl | 92-52-4 | 2.13E-05 | 9.32E-05 | 2.68E-06 | 9.32E-05 | 2.68E-06 | 8 hour | 0.000% |
| Bis(2-Ethylhexyl)phthalate | 117-81-7 | 9.14E-04 | 4.00E-03 | 1.15E-04 | 4.00E-03 | 1.15E-04 | Annual | 0.012% |
| Bromoforn | 75-25-2 | 4.89E-04 | 2.14E-03 | 6.15E-05 | 2.14E-03 | 6.15E-05 | Annual | 0.001% |
| Carbon disulfide | 75-15-0 | 1.63E-03 | 7.13E-03 | 2.09E-04 | 7.13E-03 | 2.09E-04 | 24 hour | 0.000% |
| Carbon disulfide | 75-15-0 | 1.63E-03 | 7.13E-03 | 2.09E-04 | 7.13E-03 | 2.09E-04 | Annual | 0.001% |
| Carbon tetrachloride | 56-23-6 | 4.24E-04 | 1.86E-03 | 5.35E-05 | 1.86E-03 | 5.35E-05 | Annual | 0.40% |
| Carbon tetrachloride | 56-23-6 | 1.06E-02 | 4.65E-02 | 1.34E-03 | 4.65E-02 | 1.34E-03 | Annual | 0.40% |
| Chlorine | 7782-50-5 | 8.16E-01 | 8.16E-01 | 2.35E-02 | 8.16E-01 | 2.35E-02 | 8 hour | 0.42% |
| Chlorine | 7782-50-5 | 8.16E-01 | 8.16E-01 | 2.35E-02 | 8.16E-01 | 2.35E-02 | Annual | 0.40% |
| 2-Chloroacetophenone | 532-27-4 | 8.76E-05 | 3.84E-04 | 1.10E-05 | 3.84E-04 | 1.10E-05 | 24 hour | 0.000% |
| 2-Chloroacetophenone | 532-27-4 | 8.76E-05 | 3.84E-04 | 1.10E-05 | 3.84E-04 | 1.10E-05 | 8 hour | 0.12% |
| 1,4-Dichlorobenzene | 106-46-7 | 2.50E-04 | 1.10E-03 | 3.15E-05 | 1.10E-03 | 3.15E-05 | 24 hour | 0.000% |
| 1,4-Dichlorobenzene | 106-46-7 | 2.50E-04 | 1.10E-03 | 3.15E-05 | 1.10E-03 | 3.15E-05 | Annual | 0.005% |
| 1,4-Dithinophenol | 51-28-5 | 4.24E-05 | 1.86E-04 | 5.35E-06 | 1.86E-04 | 5.35E-06 | Annual | 0.001% |
| 1,4-Dithinophenol | 51-28-5 | 4.24E-05 | 1.86E-04 | 5.35E-06 | 1.86E-04 | 5.35E-06 | Annual | 0.001% |
| 2,4-Dinitrofluorene | 121-14-2 | 3.50E-06 | 1.53E-05 | 4.42E-07 | 1.53E-05 | 4.42E-07 | 8 hour | 0.000% |
| 2,4-Dinitrofluorene | 121-14-2 | 3.50E-06 | 1.53E-05 | 4.42E-07 | 1.53E-05 | 4.42E-07 | Annual | 0.000% |
| Dimethyl sulfide | 77-78-1 | 6.01E-04 | 2.68E-03 | 7.57E-05 | 2.68E-03 | 7.57E-05 | Annual | 0.001% |
| Dimethyl sulfide | 77-78-1 | 6.01E-04 | 2.68E-03 | 7.57E-05 | 2.68E-03 | 7.57E-05 | 8 hour | 0.041% |
| Ethylbenzene | 100-41-4 | 7.31E-03 | 3.20E-02 | 9.21E-04 | 3.20E-02 | 9.21E-04 | 24 hour | 0.000% |
| Ethylbenzene | 100-41-4 | 7.31E-03 | 3.20E-02 | 9.21E-04 | 3.20E-02 | 9.21E-04 | Annual | 0.000% |
| Ethylene dichloride | 107-06-2 | 5.01E-04 | 2.19E-03 | 6.31E-05 | 2.19E-03 | 6.31E-05 | 24 hour | 0.003% |
| Ethylene dichloride | 107-06-2 | 5.01E-04 | 2.19E-03 | 6.31E-05 | 2.19E-03 | 6.31E-05 | Annual | 0.000% |
| Ethylene dibromide | 106-93-4 | 1.50E-05 | 6.58E-05 | 1.89E-06 | 6.58E-05 | 1.89E-06 | 24 hour | 0.000% |
| Ethylene dibromide | 106-93-4 | 1.50E-05 | 6.58E-05 | 1.89E-06 | 6.58E-05 | 1.89E-06 | Annual | 0.000% |
| Formaldehyde | 50-00-0 | 1.04E+00 | 4.54E+00 | 1.31E-01 | 4.54E+00 | 1.31E-01 | Annual | 34.44% |

**Northern Michigan University
New CFB Boiler
Toxic Air Contaminant Modeling Results**

1.0 Gram/Sec Modeled Impacts

| Impact | Averaging Period | (ug/hr / 1 g/s) |
|---------|------------------|-----------------|
| Annual | Annual | 0.211 |
| 24 Hour | 24 Hour | 1.589 |
| 8 Hour | 8 Hour | 2.712 |
| 1 Hour | 1 Hour | 15.779 |

| Compound | CAS No. | Emission Rates | | Modelled Rate (g/sec) | IRSL (ug/m3) | IRSL (ug/m3) | Averaging Period | Ambient Impact % of SL |
|-----------------------|------------|----------------|----------|-----------------------|--------------|--------------|------------------|------------------------|
| | | Maximum | Minimum | | | | | |
| | | (lb/hr) | (kg) | | | | | |
| Heptachloropiphenyl | 28665-71-2 | 1.56E-08 | 8.82E-08 | 1.96E-09 | 0.1 | 0.1 | Annual | 4.13E-10 |
| Hexachlorobiphenyl | 26601-64-9 | 1.30E-07 | 5.69E-07 | 1.63E-08 | 0.1 | 0.1 | Annual | 3.44E-09 |
| Hexane | 110-64-3 | 3.75E-01 | 1.64E+00 | 4.73E-02 | 2 | 2 | Annual | 4.38E-05 |
| Hexanal | 66-25-1 | 1.65E-03 | 7.23E-03 | 2.09E-04 | 0.1 | 0.1 | Annual | 3.44E-09 |
| Isophorone | 78-84-2 | 2.83E-03 | 1.24E-02 | 3.56E-04 | 160 | 160 | 24 hour | 5.66E-04 |
| Isophorone | 78-59-1 | 7.26E-03 | 3.18E-02 | 9.15E-04 | 280 | 280 | 1 hour | 1.44E-02 |
| Isophorone | 78-59-1 | 7.26E-03 | 3.18E-02 | 9.15E-04 | 280 | 280 | 1 hour | 1.44E-02 |
| 2-Methylpropanthrene | 91-57-8 | 3.77E-05 | 1.65E-04 | 4.75E-06 | 10 | 10 | Annual | 1.03E-06 |
| 2-Methylpropanthrene | 91-57-8 | 3.77E-05 | 1.65E-04 | 4.75E-06 | 10 | 10 | Annual | 1.03E-06 |
| Methoxychlorobiphenyl | 74-83-9 | 5.19E-08 | 2.27E-07 | 6.53E-09 | 0.1 | 0.1 | Annual | 1.38E-09 |
| Methoxychlorobiphenyl | 74-83-9 | 5.19E-08 | 2.27E-07 | 6.53E-09 | 0.1 | 0.1 | Annual | 1.38E-09 |
| Methyl bromide | 74-83-9 | 3.54E-03 | 1.55E-02 | 4.46E-04 | 5 | 5 | 24 hour | 7.08E-04 |
| Methyl chloride | 74-87-3 | 6.63E-03 | 2.91E-02 | 8.36E-04 | 90 | 90 | 24 hour | 1.33E-03 |
| Methyl chloride | 74-87-3 | 6.63E-03 | 2.91E-02 | 8.36E-04 | 90 | 90 | 24 hour | 1.33E-03 |
| Methyl ethyl ketone | 78-93-3 | 4.86E-03 | 2.14E-02 | 6.15E-04 | 5000 | 5000 | 24 hour | 9.77E-04 |
| Methyl hydrazine | 60-34-4 | 2.15E-03 | 9.32E-03 | 2.68E-04 | 0.1 | 0.1 | Annual | 5.65E-05 |
| Methyl isobutyl ether | 1634-04-4 | 4.36E-04 | 1.92E-03 | 5.52E-05 | 3000 | 3000 | 24 hour | 8.77E-05 |
| Methyl isobutyl ether | 1634-04-4 | 4.36E-04 | 1.92E-03 | 5.52E-05 | 3000 | 3000 | 24 hour | 8.77E-05 |
| Methyl methacrylate | 80-62-6 | 2.50E-04 | 1.10E-03 | 3.15E-05 | 700 | 700 | 24 hour | 5.01E-05 |
| Methyl methacrylate | 80-62-6 | 2.50E-04 | 1.10E-03 | 3.15E-05 | 700 | 700 | 24 hour | 5.01E-05 |
| Propionaldehyde | 123-58-6 | 7.54E-04 | 3.30E-03 | 9.61E-05 | 4 | 4 | Annual | 3.82E-04 |
| Propionaldehyde | 123-58-6 | 7.54E-04 | 3.30E-03 | 9.61E-05 | 4 | 4 | Annual | 3.82E-04 |
| Phenol | 108-95-2 | 1.20E-02 | 5.27E-02 | 1.51E-03 | 600 | 600 | 1 hour | 2.39E-02 |
| Phenol | 108-95-2 | 1.20E-02 | 5.27E-02 | 1.51E-03 | 600 | 600 | 1 hour | 2.39E-02 |
| Pentachlorophenol | 87-66-5 | 1.23E-07 | 5.37E-07 | 1.64E-08 | 0.1 | 0.1 | Annual | 3.25E-09 |
| Pentachlorophenol | 87-66-5 | 1.23E-07 | 5.37E-07 | 1.64E-08 | 0.1 | 0.1 | Annual | 3.25E-09 |
| Pentachlorophenol | 87-66-5 | 1.20E-05 | 6.27E-05 | 1.87E-06 | 100 | 100 | 24 hour | 3.19E-07 |
| Pentachlorophenol | 87-66-5 | 1.20E-05 | 6.27E-05 | 1.87E-06 | 100 | 100 | 24 hour | 3.19E-07 |
| Styrene | 100-42-5 | 4.48E-01 | 1.96E+00 | 5.64E-02 | 4 | 4 | Annual | 2.09E-05 |
| Styrene | 100-42-5 | 4.48E-01 | 1.96E+00 | 5.64E-02 | 4 | 4 | Annual | 2.09E-05 |
| Styrene | 100-42-5 | 4.48E-01 | 1.96E+00 | 5.64E-02 | 4 | 4 | Annual | 2.09E-05 |
| Styrene | 100-42-5 | 4.48E-01 | 1.96E+00 | 5.64E-02 | 4 | 4 | Annual | 2.09E-05 |
| Toluene | 108-88-3 | 2.17E-01 | 9.50E-01 | 2.73E-02 | 5000 | 5000 | 24 hour | 4.34E-02 |
| Toluene | 108-88-3 | 2.17E-01 | 9.50E-01 | 2.73E-02 | 5000 | 5000 | 24 hour | 4.34E-02 |
| p-Tolualdehyde | 529-20-4 | 1.70E-03 | 7.43E-03 | 2.14E-04 | 440 | 440 | 24 hour | 3.40E-04 |
| p-Tolualdehyde | 529-20-4 | 1.70E-03 | 7.43E-03 | 2.14E-04 | 440 | 440 | 24 hour | 3.40E-04 |
| p-Tolualdehyde | 104-87-0 | 2.59E-03 | 1.14E-02 | 3.27E-04 | 0.1 | 0.1 | Annual | 6.89E-05 |
| p-Tolualdehyde | 104-87-0 | 2.59E-03 | 1.14E-02 | 3.27E-04 | 0.1 | 0.1 | Annual | 6.89E-05 |
| Trichloroethylene | 75-69-4 | 6.13E-07 | 2.68E-06 | 7.22E-08 | 0.1 | 0.1 | Annual | 1.63E-08 |
| Trichloroethylene | 75-69-4 | 6.13E-07 | 2.68E-06 | 7.22E-08 | 0.1 | 0.1 | Annual | 1.63E-08 |
| Trichloroethylene | 79-01-6 | 7.07E-03 | 3.10E-02 | 8.91E-04 | 56200 | 56200 | 1 hour | 1.92E-02 |
| Trichloroethylene | 79-01-6 | 7.07E-03 | 3.10E-02 | 8.91E-04 | 56200 | 56200 | 1 hour | 1.92E-02 |
| 2,4,6-Trichlorophenol | 88-06-2 | 5.19E-06 | 2.27E-05 | 6.63E-07 | 1000 | 1000 | 24 hour | 1.46E-03 |
| 2,4,6-Trichlorophenol | 88-06-2 | 5.19E-06 | 2.27E-05 | 6.63E-07 | 1000 | 1000 | 24 hour | 1.46E-03 |
| Vinyl acetate | 108-05-4 | 9.51E-04 | 4.17E-03 | 1.20E-04 | 200 | 200 | 24 hour | 1.38E-07 |
| Vinyl acetate | 108-05-4 | 9.51E-04 | 4.17E-03 | 1.20E-04 | 200 | 200 | 24 hour | 1.38E-07 |
| Vinyl Chloride | 75-01-4 | 4.24E-03 | 1.86E-02 | 5.35E-04 | 100 | 100 | 24 hour | 8.50E-04 |
| Vinyl Chloride | 75-01-4 | 4.24E-03 | 1.86E-02 | 5.35E-04 | 100 | 100 | 24 hour | 8.50E-04 |
| Xylenes | 1330-20-7 | 4.63E-04 | 2.03E-03 | 5.93E-05 | 100 | 100 | 24 hour | 9.27E-05 |
| Xylenes | 1330-20-7 | 4.63E-04 | 2.03E-03 | 5.93E-05 | 100 | 100 | 24 hour | 9.27E-05 |
| o-Xylene | 95-47-6 | 5.89E-03 | 2.58E-02 | 7.43E-04 | 100 | 100 | 24 hour | 1.18E-03 |
| o-Xylene | 95-47-6 | 5.89E-03 | 2.58E-02 | 7.43E-04 | 100 | 100 | 24 hour | 1.18E-03 |

Polynuclear Aromatic Hydrocarbons (PAH)

Note: An IRSL of 0.1 that is red bolded is a default screening level per AQI air toxics policy